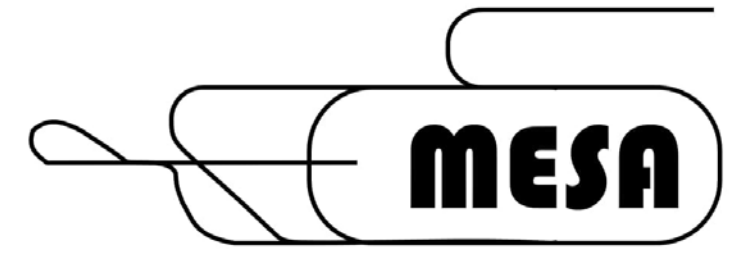


STATUS OF SUPERCONDUCTING THIN FILMS ON HIGHER ORDER MODE ANTENNAS FOR MESA

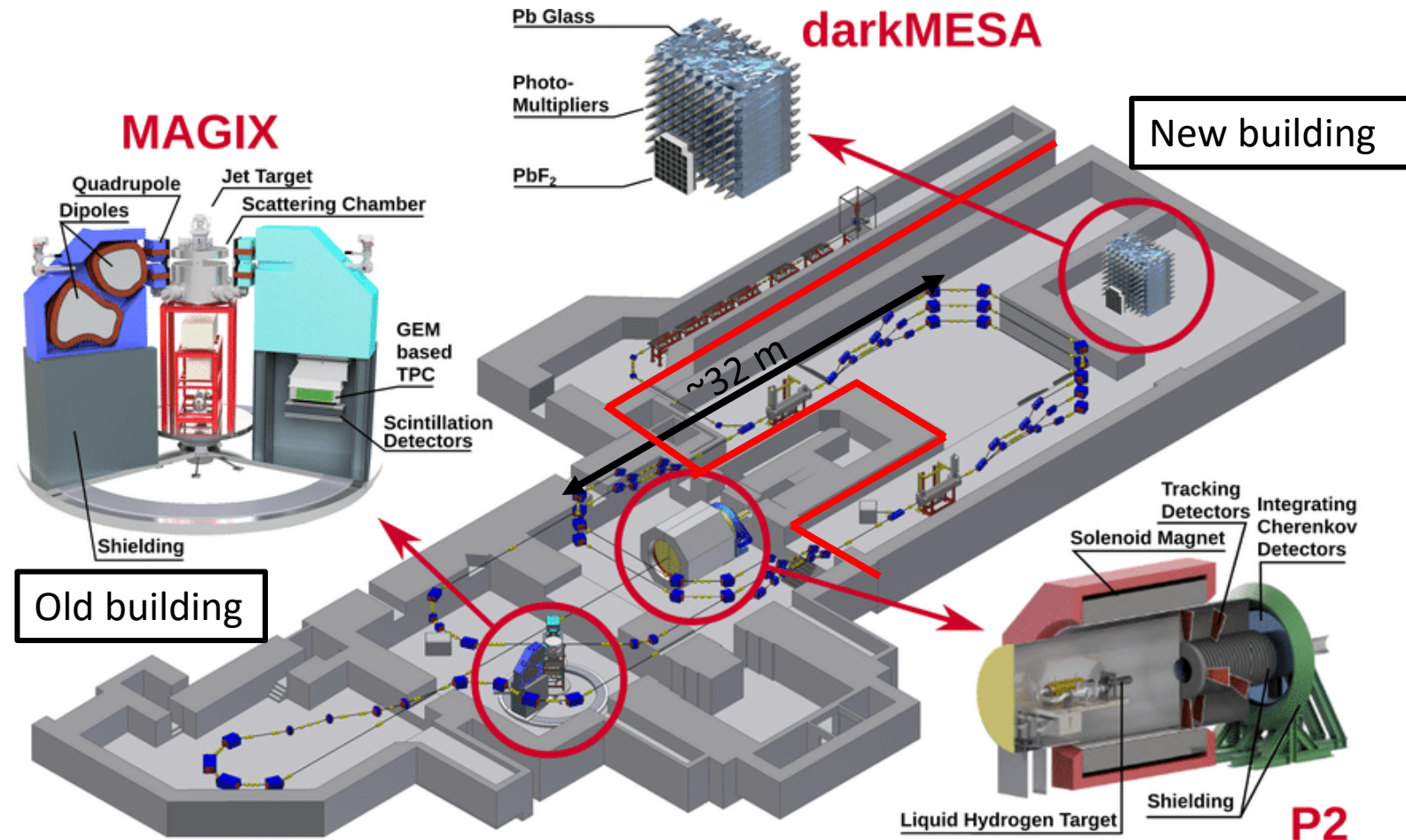
Florian Hug, Paul Plattner, Timo Stengler
Institut für Kernphysik
JGU Mainz
27.09.2024



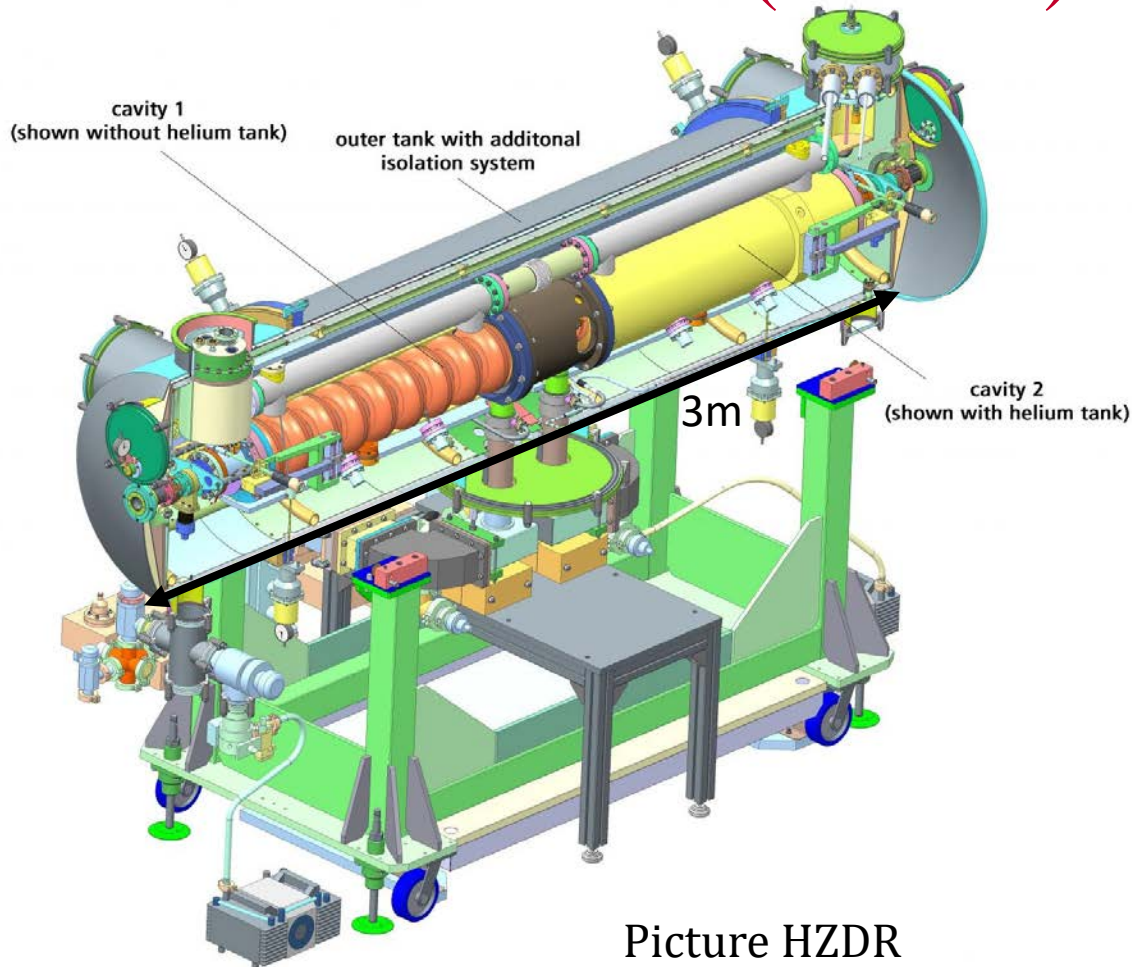
MAINZ ENERGY-RECOVERING SUPERCONDUCTING ACCELERATOR

Injector NC	5 MeV
Cryomodules SC	25 MeV
EB-mode P2	155 MeV @ 150 μ A (pol.)
ER-mode MAGIX	105 MeV @ 1 (10) mA
Q_0	$1.25 * 10^{10}$
f	1.3 GHz

Talk from T. Stengler (TU005)



MESA ENHANCED ELBE-TYPE CRYOMODULES (MEEC)



2 Cryomodule of the „Rossendorf“-type (2x 9-Cell TESLA/XFEL cavities) fabricated by Research Instruments (RI)

Specific modification for MESA:

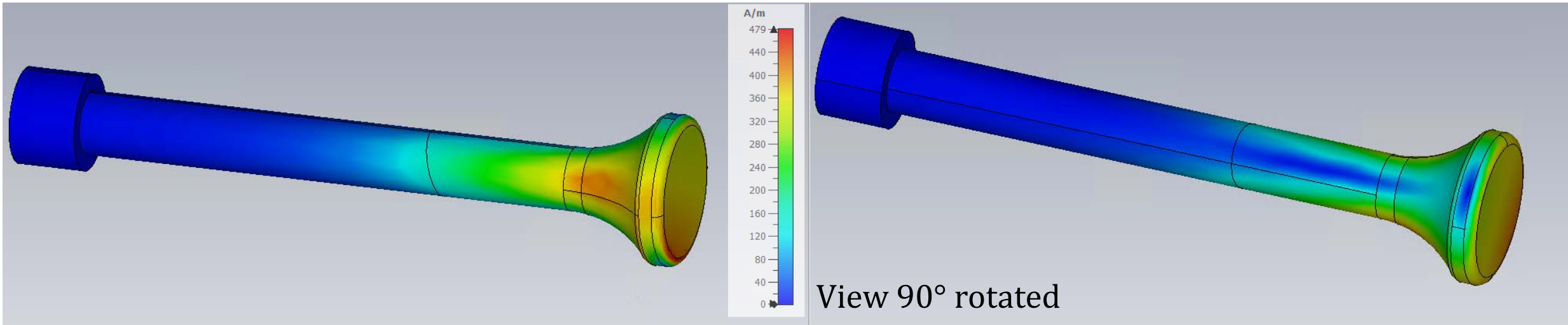
- Piezo tuner (XFEL/Saclay)
- Sapphire ceramic for HOM-antenna
- Optimized cooling of HOM RF-cable
- Modified LHe-port for the Joule-Thomson valve

→ Two MESA Cryomodules are onsite and tested
→ ALICE Module (spare/testing)*
→ Further optimisation for beam current at 10 mA

*We would like to thank STFC Daresbury for their generous gift.

MAGNETIC FIELD AT ANTENNA

$$H_{\max,T} = 1\% H_{\text{peak}}$$
$$E_{\text{acc}} = 12.5 \frac{\text{MeV}}{\text{m}}$$



Maximum of magnetic field at antenna $H_{\max,T} = 0.53 \text{ mT}$

Field distribution: maximum at the tip of the antenna

Field maxima of HOMs not at tip and $H_{\max,\text{HOM}} < H_{\max,T}$

$$H_{\max,\text{HOM}} / H_{\max,T} \approx 0.001 \text{ for strongest dipole mode}$$

POWER LOSS AT ANTENNA TIP

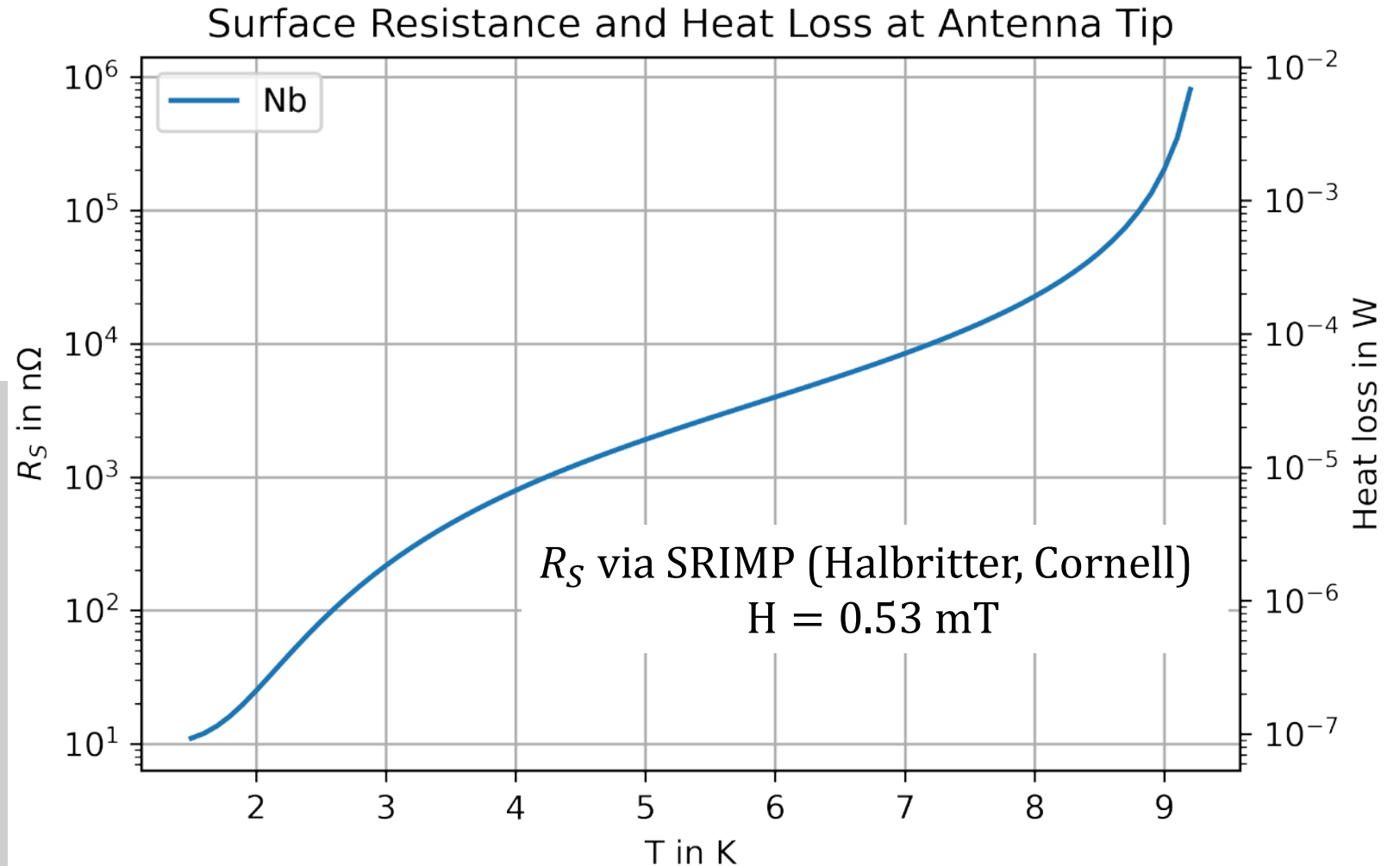
Material	Nb
T_C / K	9.27
F / GHz	1.3
λ_L / nm	39
ξ / nm [1]	380
$\Delta_{reduced}$ [2]	1.5

[1] all values are multiplied by $\frac{\pi}{2}$
 [2] all values are multiplied by $\frac{1.60218 \cdot 10^{-22}}{k_B \cdot T_{C,i}}$

Heat loss at the antenna can be calculated via R_S :

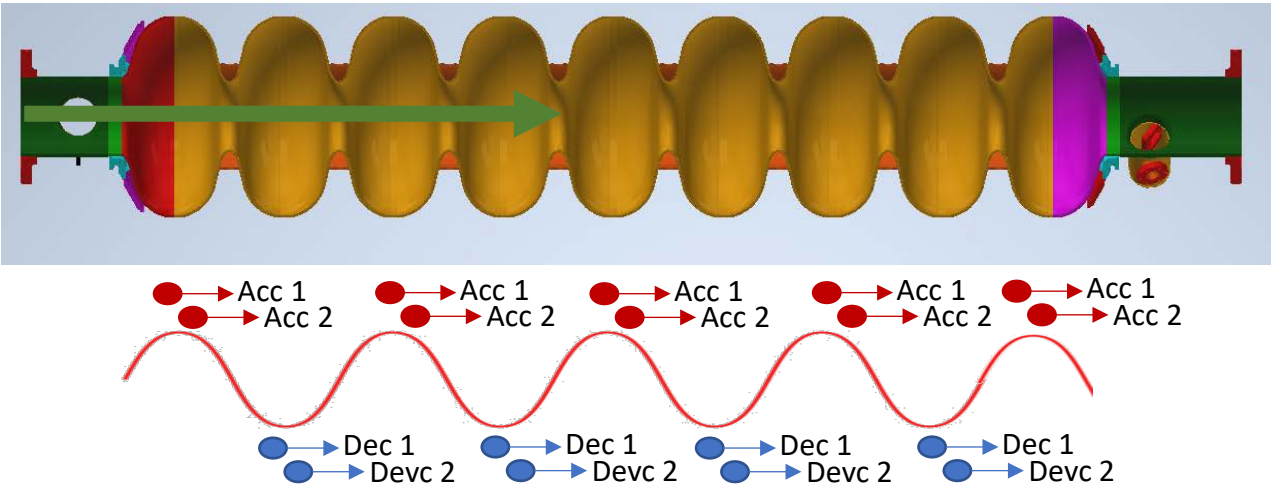
$$P_{loss} = \frac{1}{2} R_S \int |H|^2 ds$$

Dominated by 1.3 GHz
 Beam-cavity interaction neglected!



HIGHER ORDER MODES - BEAM INDUCED HOMS

In ERL-mode: 4 e- beams simultaneous
(2x accelerating; 2x decelerating)



Power stored in HOMs (longitudinal):

$$P_{HOM} = N * q * k * I$$

N: #beams; q: bunch charge; k: loss factor; I: average beam current

→ 30% of P_{HOM} at HOM antenna tip

L. Merminga, D.R. Douglas, and G.A. Krafft. High-current energyrecovering electron Linacs. Annual Review of Nuclear and Particle Science, 53(1):387–429, 2003.

Simulated Beam Blow Up limit: **12 mA** (C. Stoll, Phd. Thesis, 2020 Mainz)

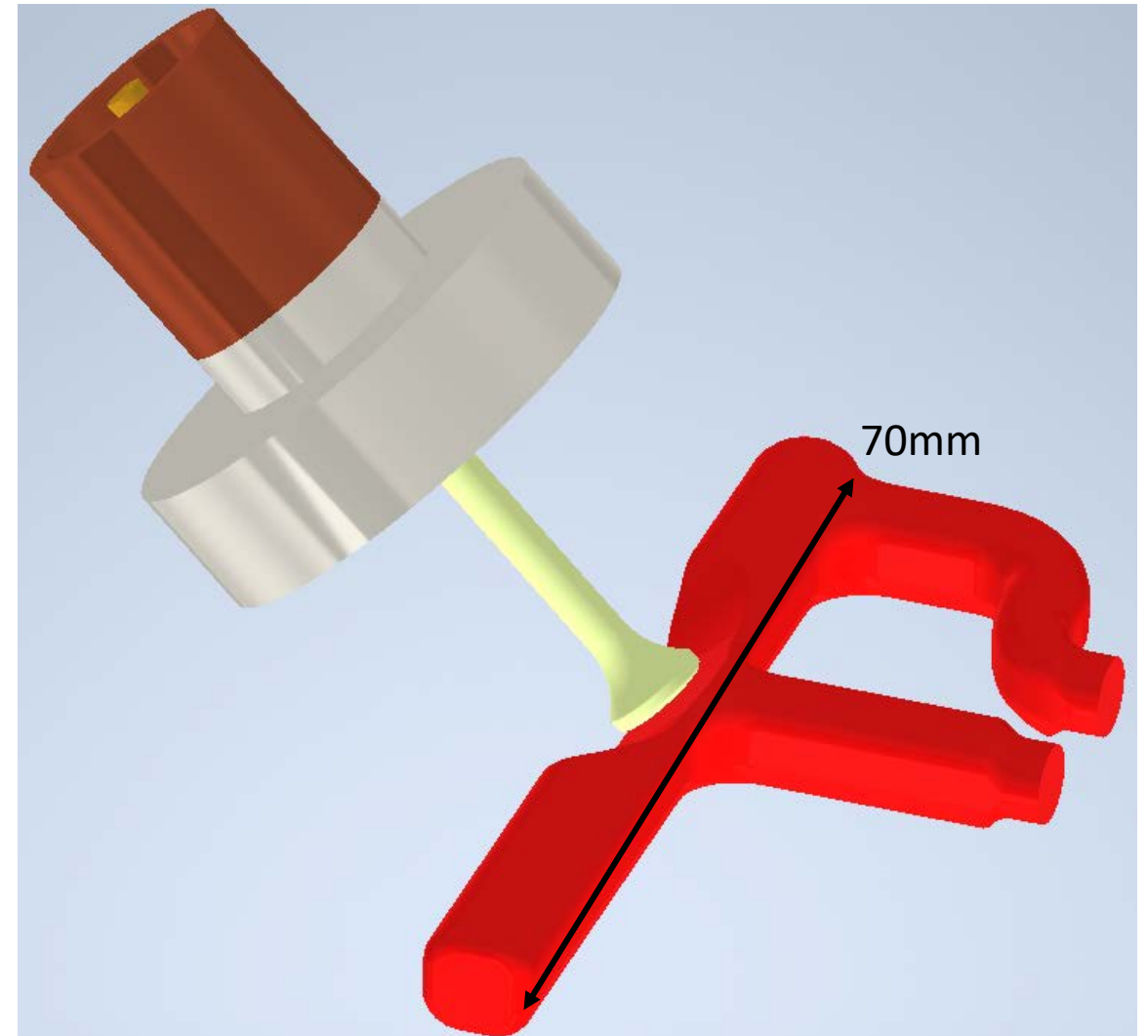
Calculated thermal power limit: **95 mW**
(~**3.2 mA**) (T. Stengler, Phd Thesis, 2020 Mainz)

I [mA]	q [pC]	P_{HOM} [mW]	P_{Tip} [mW]
1	0.7	30.8	10
10	7.7	3080	1000

HIGHER ORDER MODES – GEOMETRICAL BOUNDARIES

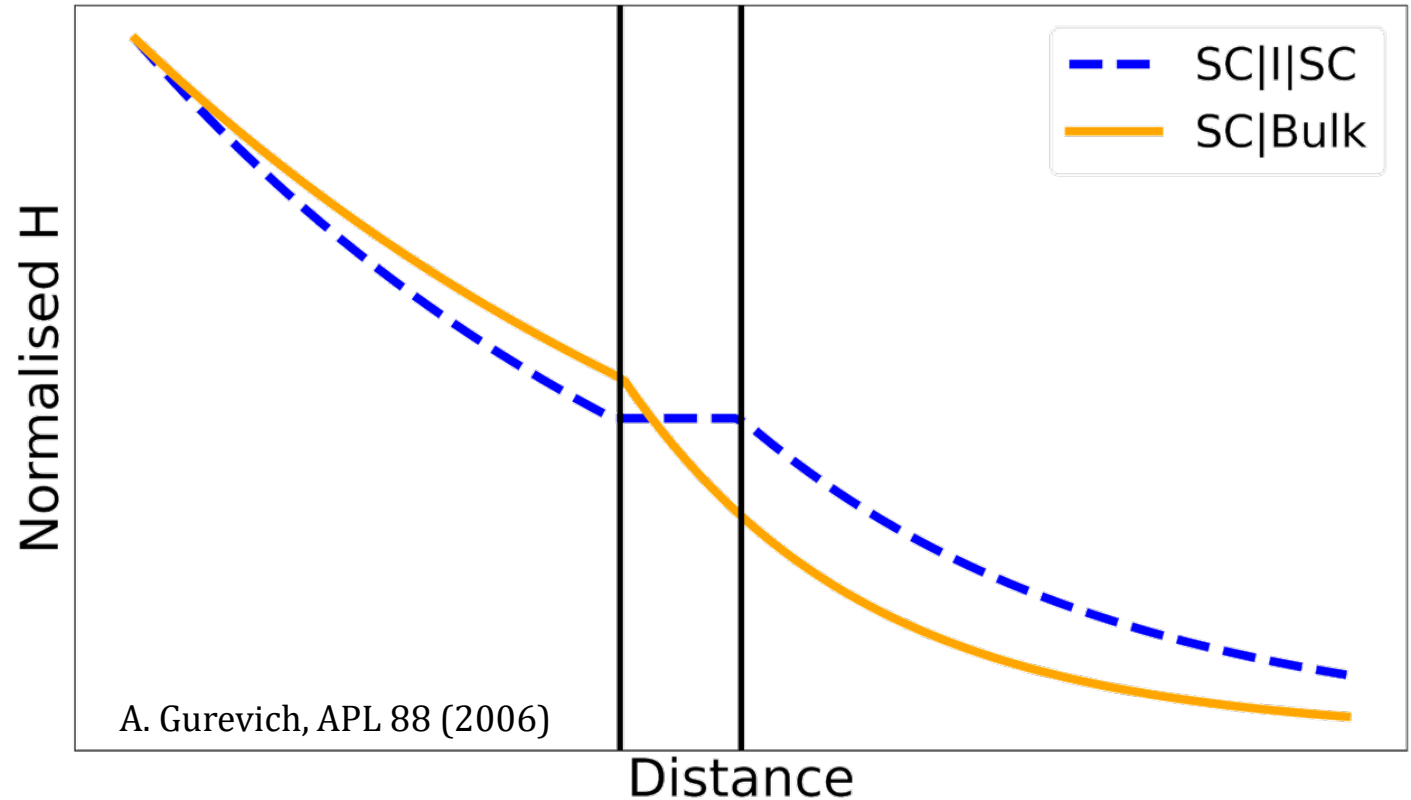
How to handle 1000 mW?

- Geometrical design of HOM antenna and F-part cannot be changed
- Minimal invasive change:
- Change the surface material to a higher T_C superconductor



SC THIN FILMS

Thin Film	Nb ₃ Sn	($d > \lambda_L$)
Bulk	OFHC-Cu	(region mm)
Thin Film	NbTiN	($d < \lambda_L$)
Insulator	AlN	(15 nm)
Bulk	Nb	(region mm)



Decision for HOM antenna:

- Coating on Nb and OFHC Cu substrates
- Complex multilayer structure not necessary (no high field region)

SC	T _c / K	λ _L / nm
Nb	9.2	39
NbTiN	17.3	150-200
Nb ₃ Sn	18.3	80-100

A-M Valente-Feliciano 2016 *Supercond. Sci. Technol.* **29** 113002 DOI 10.1088/0953-2048/29/11/113002

POWER LOSS AT ANTENNA TIP

Material	Nb	NbTiN	Nb ₃ Sn
T_C / K	9.27	17.3	18
F / GHz	1.3	1.3	1.3
λ_L / nm	39	240	90
ξ / nm [1]	380	50	70
$\Delta_{reduced}$ [2]	1.5	2.8	3.1

[1] all values are multiplied by $\frac{\pi}{2}$

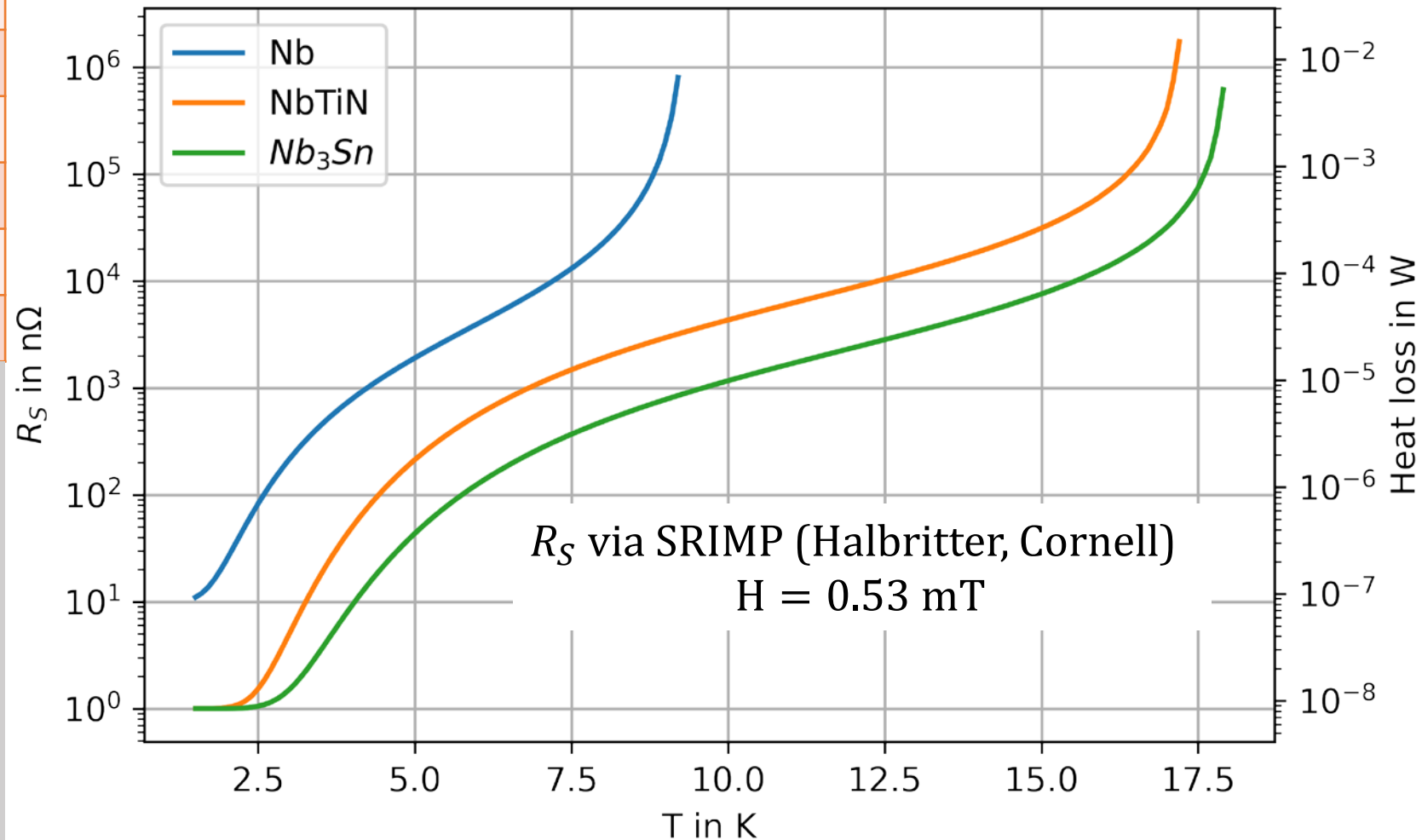
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Heat loss at the antenna can be calculated via R_S :

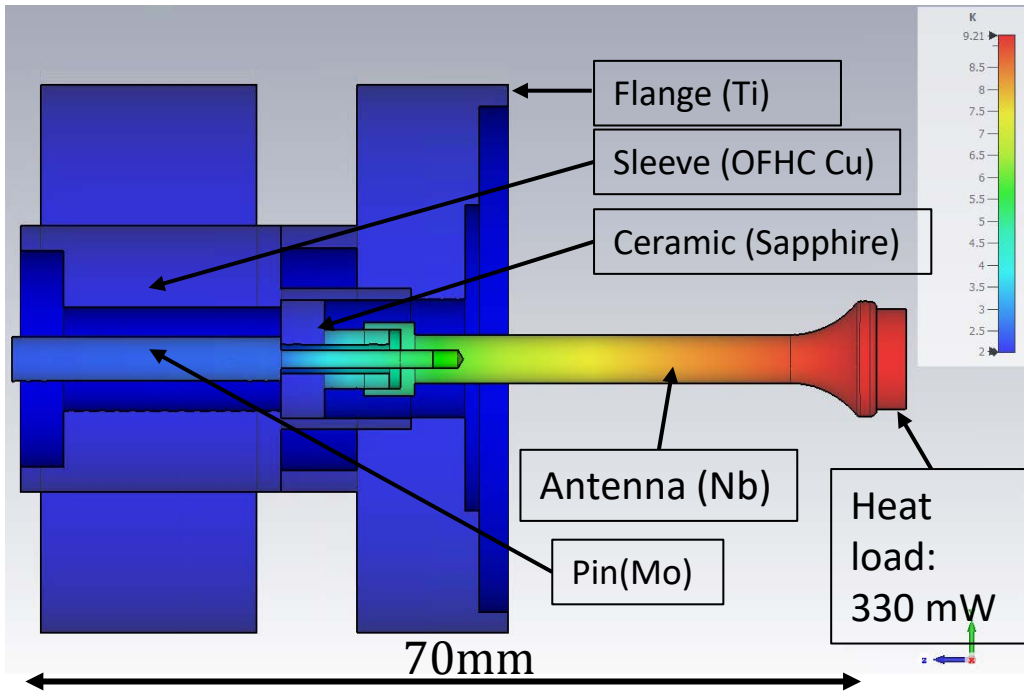
$$P_{loss} = \frac{1}{2} R_S \int |H|^2 ds$$

Dominated by 1.3 GHz
Beam-cavity interaction neglected!

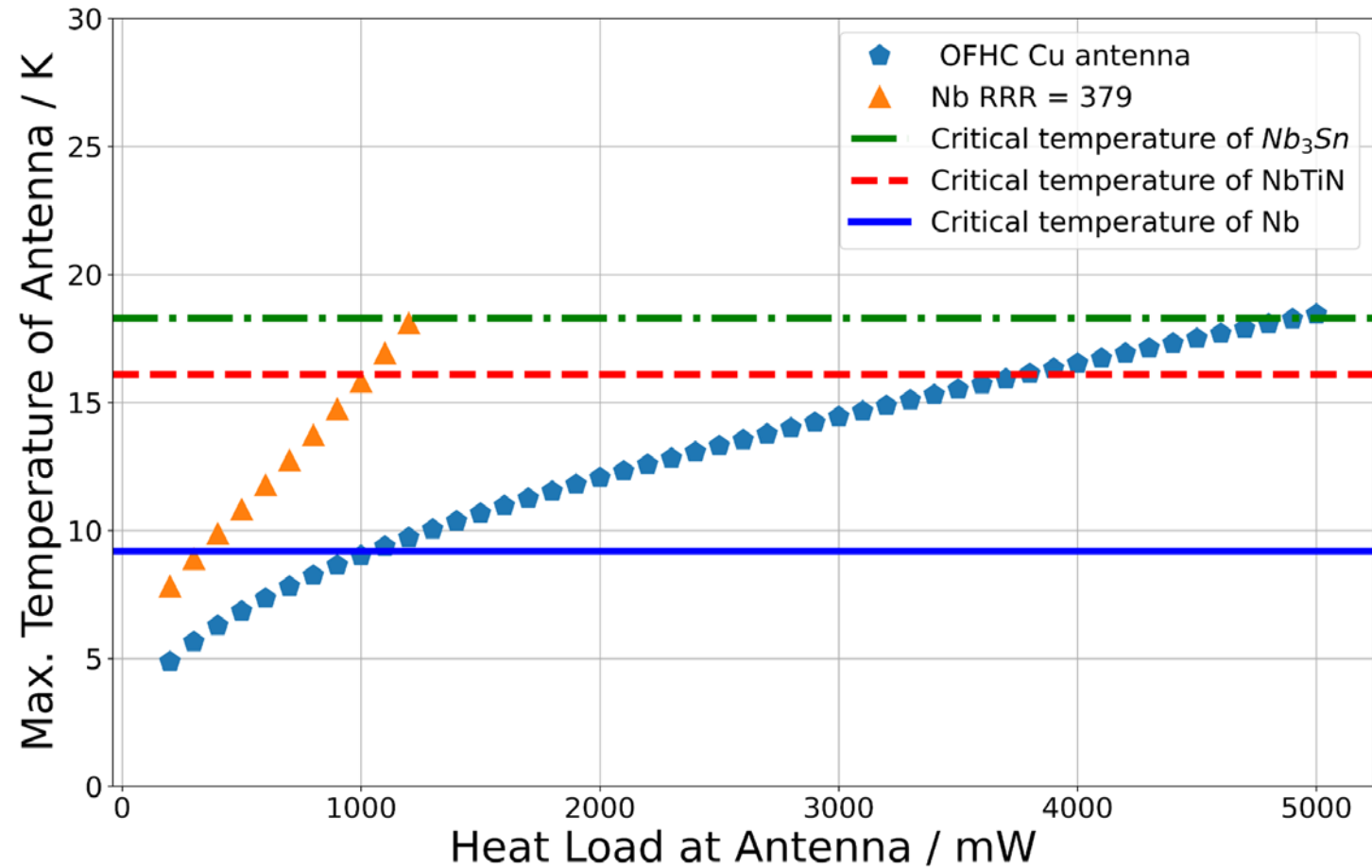
Surface Resistance and Heat Loss at Antenna Tip



CST RESULTS



Thermal properties are dominated by the bulk material (Nb, Cu)



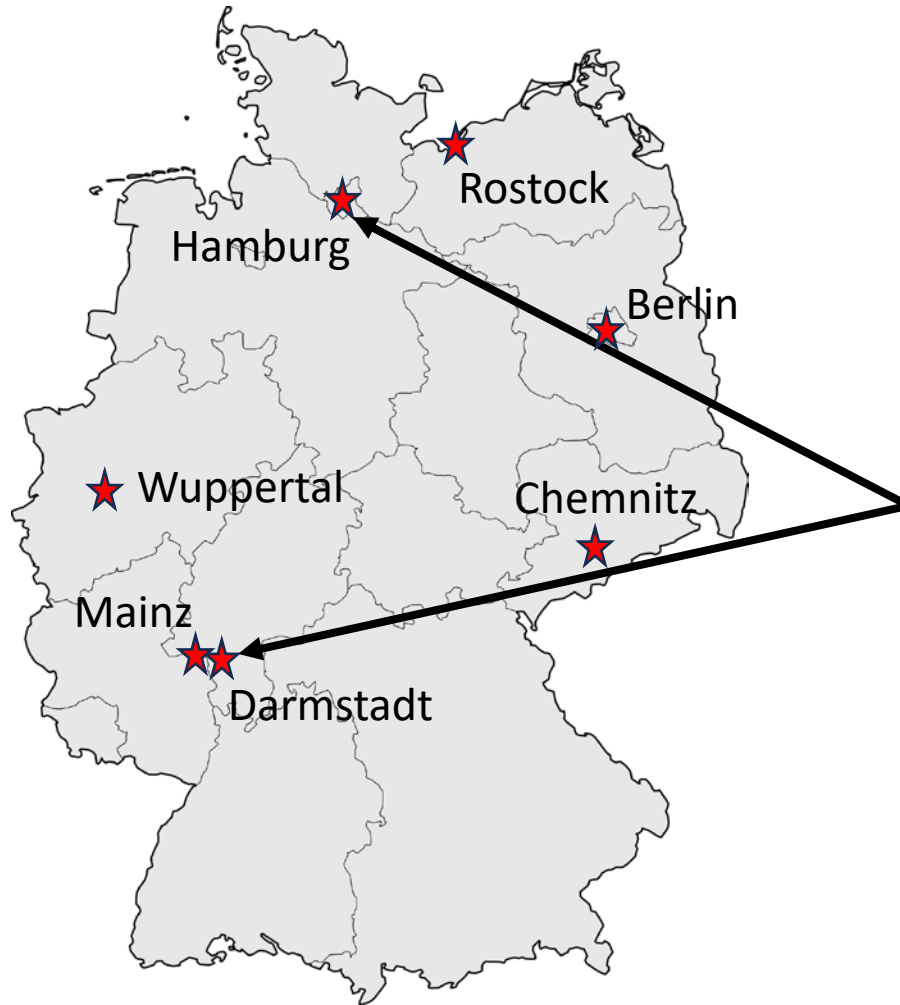
Nb antenna:

- $T_{\text{antenna}}(\sim 1000\text{mW}(\approx 10.4\text{ mA})) = T_{C,\text{NbTiN}}$

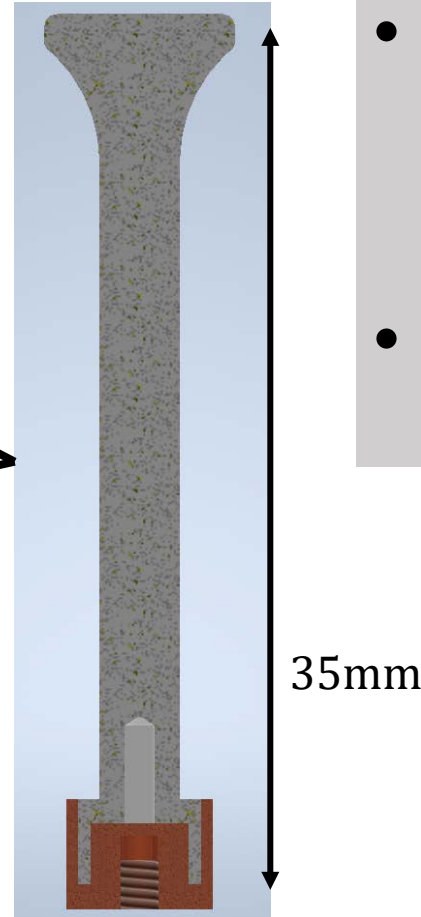
Cu antenna:

- $T_{\text{antenna}}(\sim 4700\text{mW}(\approx 22.5\text{ mA})) = T_{\text{Nb}_3\text{Sn}}$

SC THIN FILMS – TOSCA/SUPER SURFER



https://upload.wikimedia.org/wikipedia/commons/thumb/e/e3/Karte_Deutschland.svg/1513px-Karte_Deutschland.svg.png



- UHH: NbTiN on Nb (SIS possible)
Plasma Enhanced Atomic Layer
Deposition (PEALD)
- TUDA: Nb₃Sn on OFHC Cu
Co-Sputtering



SC THIN FILMS – NBTIN ON HOM ANTENNA

NbTiN (PEALD) @Hamburg

Substrate: Niobium

Time: 4 days

Thickness: $\sim 50\text{nm}$ ($< \lambda_L$)

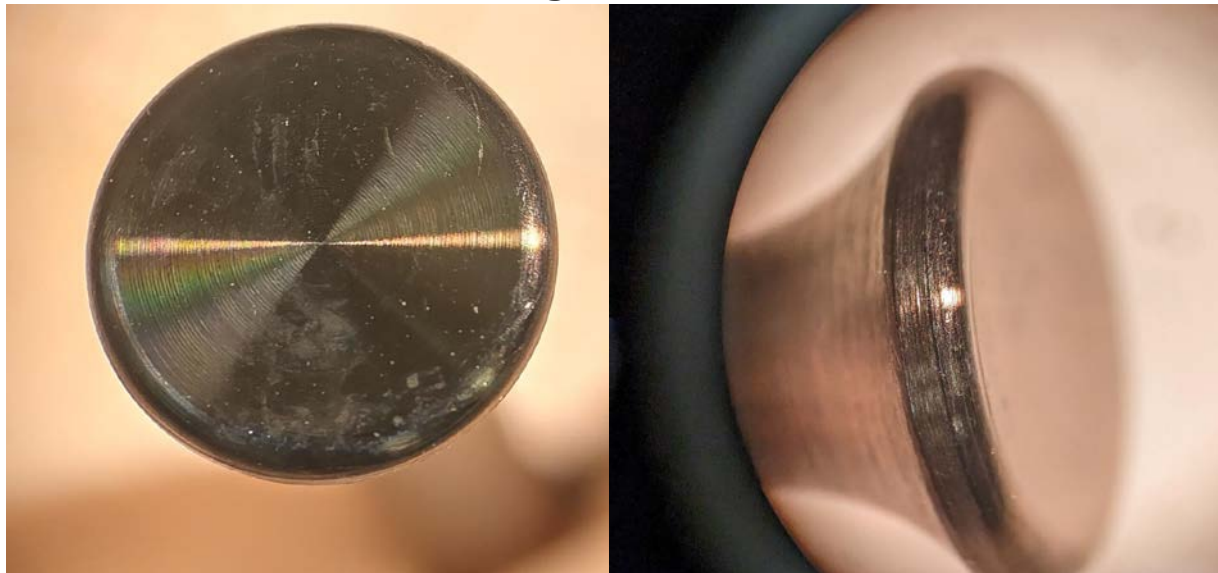
$T_C = 16\text{ K}$ (on flat samples)

Deposition Temperatur $< 300^\circ\text{C}$

→ Slow Thermal Annealing at 900°C



Universität Hamburg
DER FORSCHUNG | DER LEHRE | DER BILDUNG



Nb₃Sn (Co-Sputtering) @TU Darmstadt

Substrate: Copper

Time: 1 hour

Thickness: $\sim 400\text{nm}$ ($\geq \lambda_L$)

$T_C = \sim 14\text{ K}$ (on cylindrical substitute)

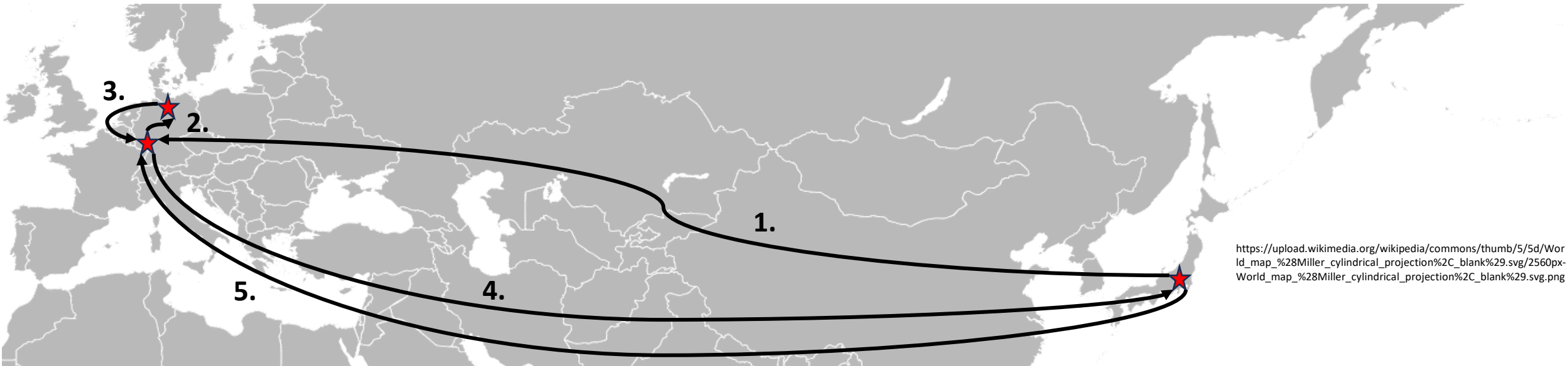
Deposition Temperatur 520°C



Picture: Amir Fahood



THE JOURNEY OF A NBTIN COATED ANTENNA



1. KYOCERA in Japan → Mainz: production of Nb antenna
2. Mainz → UHH: NbTiN coating (currently here!)
3. UHH → Mainz
4. Mainz → KYOCERA for brasing
5. KYOCERA → Mainz for testing in cavities

REFURBISHMENT OF AN ELBE-TYPE CRYOMODULE

Personal entrance (ISO 6)

Material entrance (ISO 7)

Clean room 1 (ISO 6)

Ultrasonic bath (USB) system

High pressure rinse (HPR)

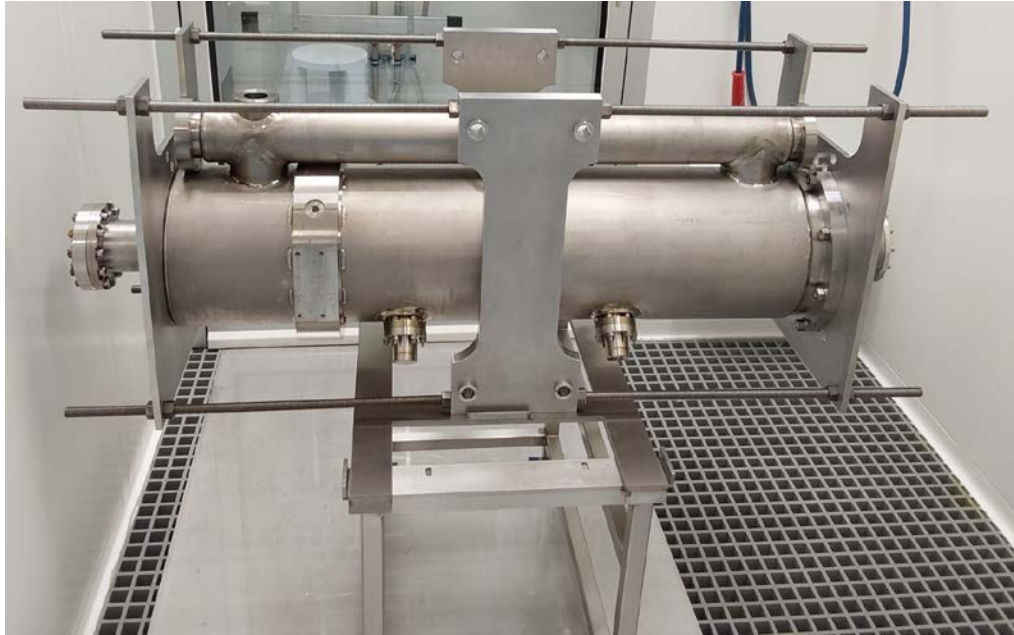
Personal airlock

Material gate

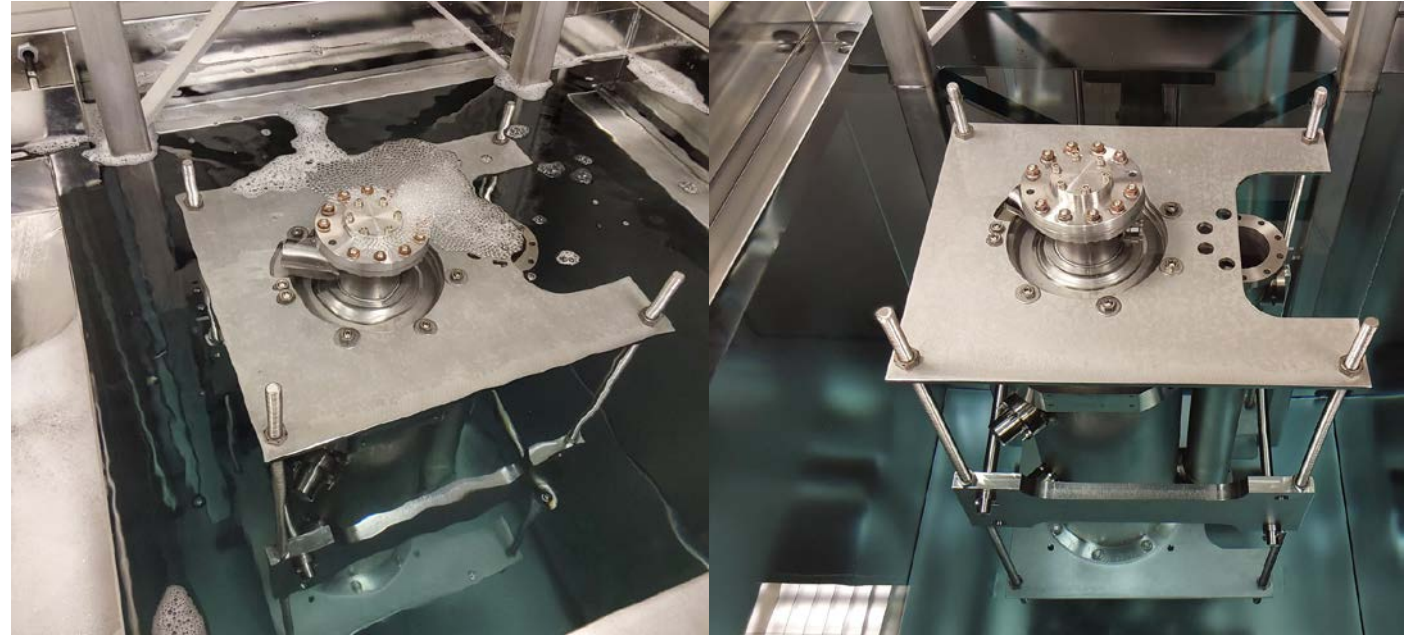
Clean room 2 (ISO 4)



REFURBISHMENT OF AN ELBE-TYPE CRYOMODULE



Material entrance



Ultrasonic bath (USB) system:

- 30 min USB with Tickopur R33
- Rinsing with ultrapure water $< 0.18 \mu\text{S}$

REFURBISHMENT OF AN ELBE-TYPE CRYOMODULE



HPR: (TESLA recipe)
each cell rinsed for 5 min (18x)



Drying for ~24 hour after HPR

Next steps:

- Installing accessories
- Vacuum with RGA
- Cold test at ATMF (baseline)

- 2nd cold test with coated HOM antennas 2025
- Assembling of the CM
- Test CM with e- beam (2026)

SUMMARY & OUTLOOK

Summary:

- Beam induced HOM power will exceed the power limit of the HOM antennas with the 10 mA upgrade at MESA

$$P_{HOM,B} = 1000 \text{ mW} > P_{MESA,lim} = 95 \text{ mW}$$

- SC Thin Films of NbTiN and Nb₃Sn will **increase the limit**

SUMMARY & OUTLOOK

Summary:

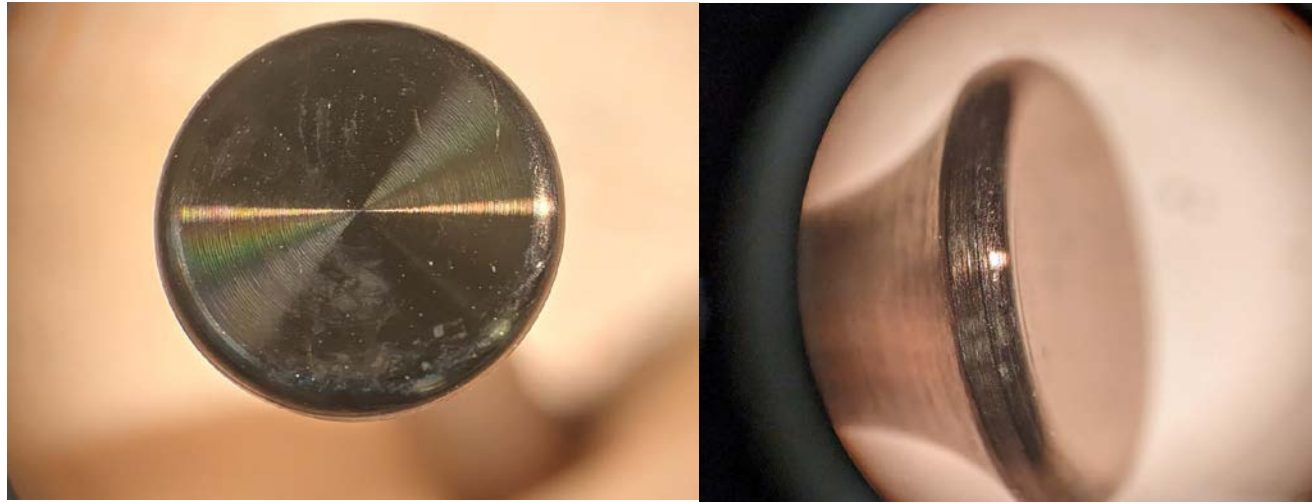
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$$P_{HOM,B} = 1000 \text{ mW} > P_{MESA,lim} = 95 \text{ mW}$$

- SC Thin Films of NbTiN and Nb₃Sn will **increase the limit**

Outlook:

- Refurbishment of 2 9-cell TESLA cavities is ongoing (MESA-ERL-test CM)
- Coating of antennas ongoing
- Cavity performance test via VCT
- CST simulation for HOM heating/ wake field ()

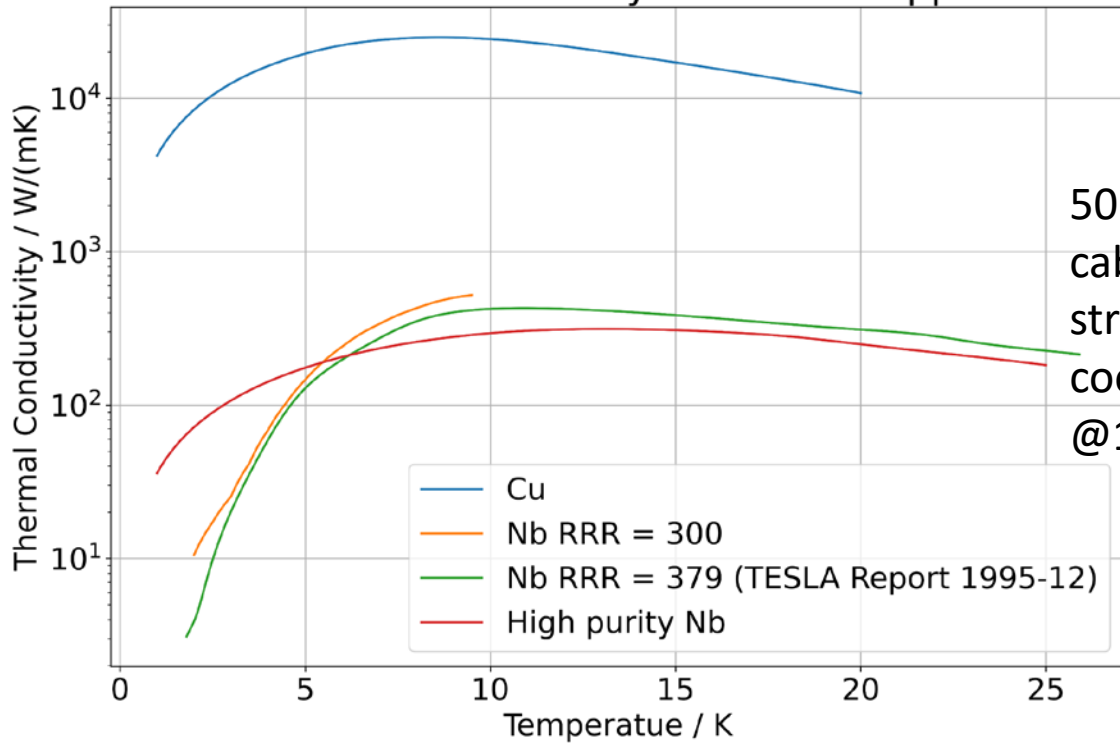


Thank you for your attention!

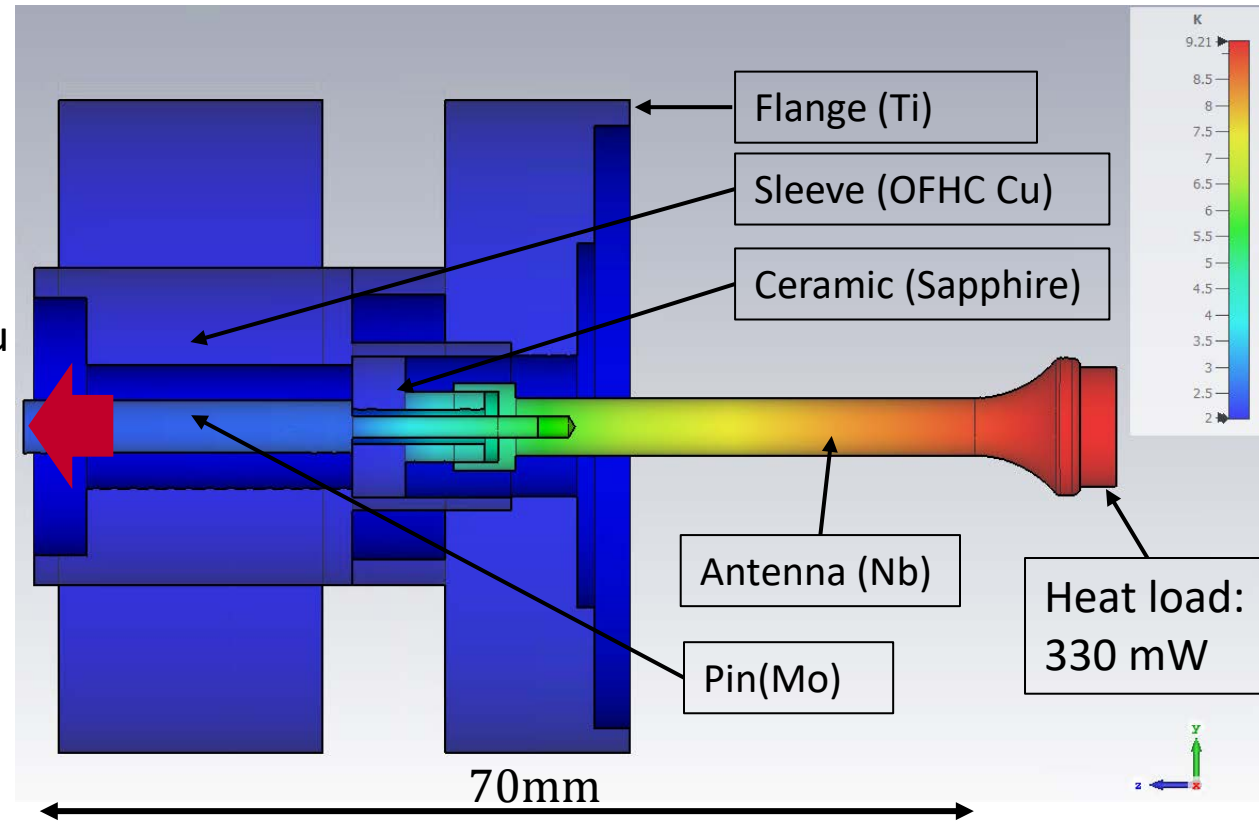
Work supported by BMBF through 05H21UMRB1.

SC THIN FILMS

Thermal Conductivity of Nb and Copper



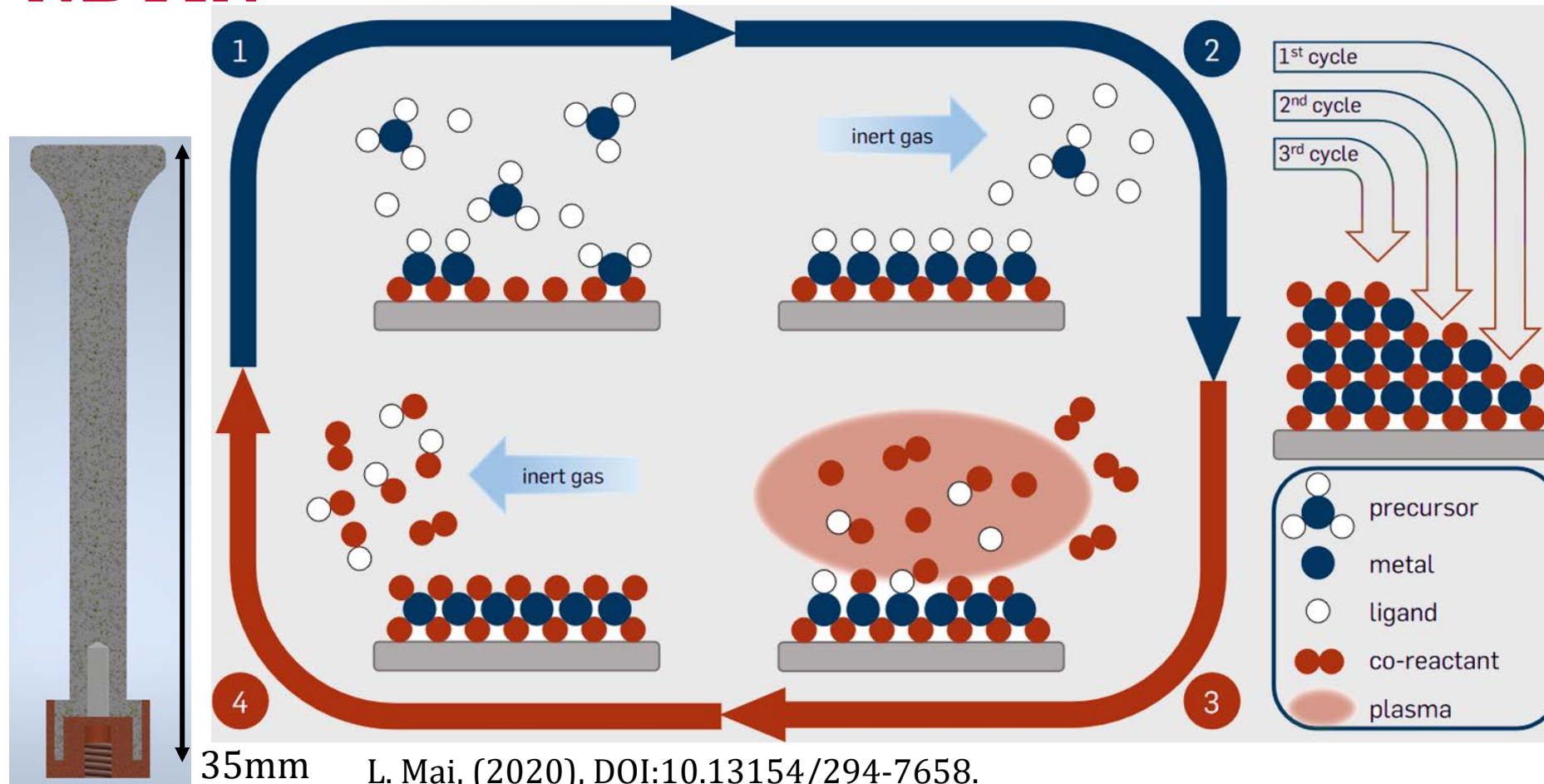
50 cm Cu cable to stripline cooler @1.8K



Material	$\kappa@2K$ [W/mK]
Nb	70
Cu	8400

Thermal Conductivity of the Elements
 C. Y. Ho, R. W. Powell and P. E. Liley
 Journal of Physical and Chemical Reference
 Data 1, 279 (1972);
<https://doi.org/10.1063/1.3253100>

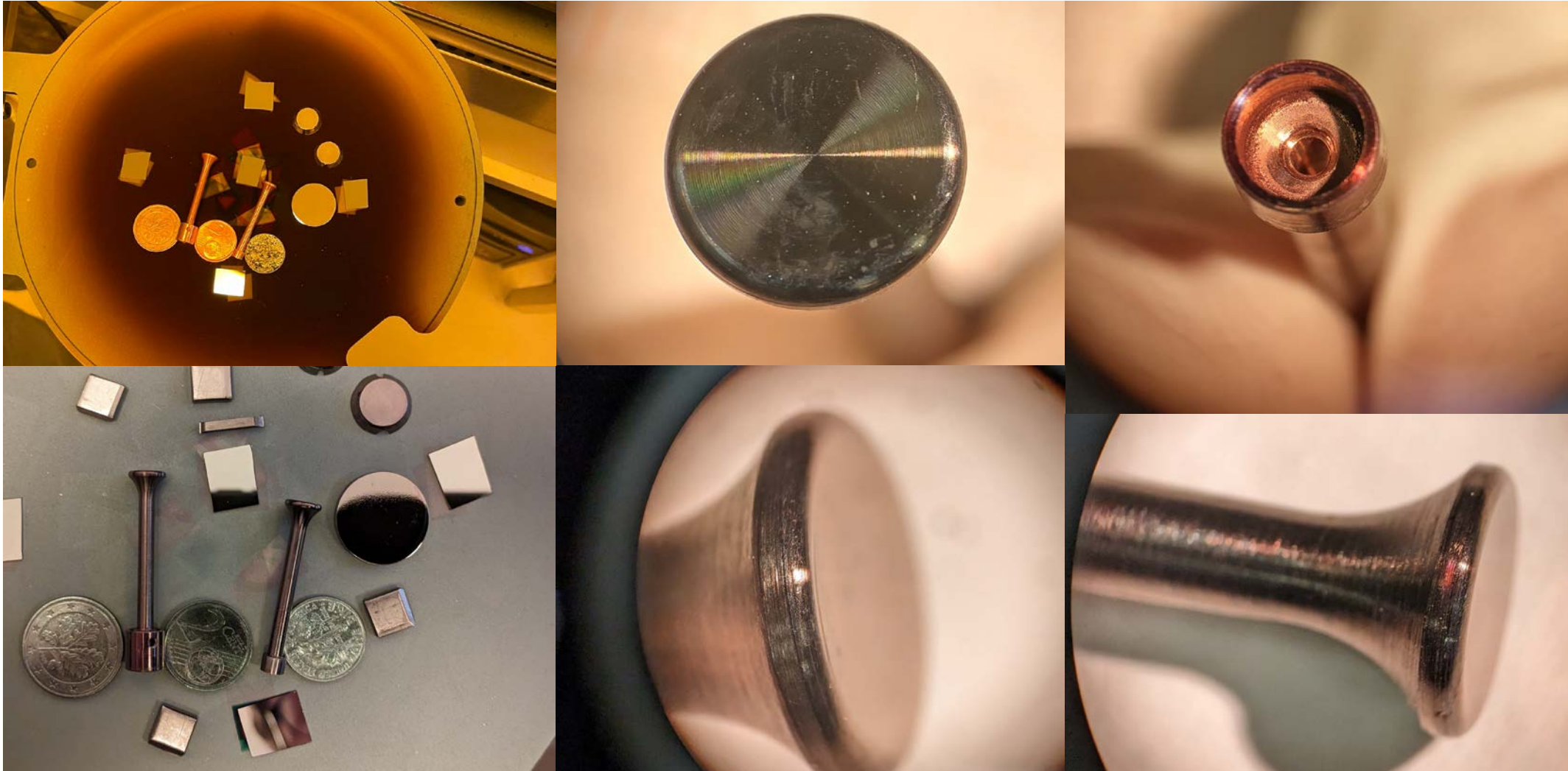
SC THIN FILMS – PLASMA-ENHANCED ALD (PEALD) NBTIN



- lower deposition temperature (<math><300\text{ }^\circ\text{C}</math>)
- higher film quality

→ Slow Thermal Annealing (STA) at 900°C

SC THIN FILMS – NBTIN ON HOM ANTENNA



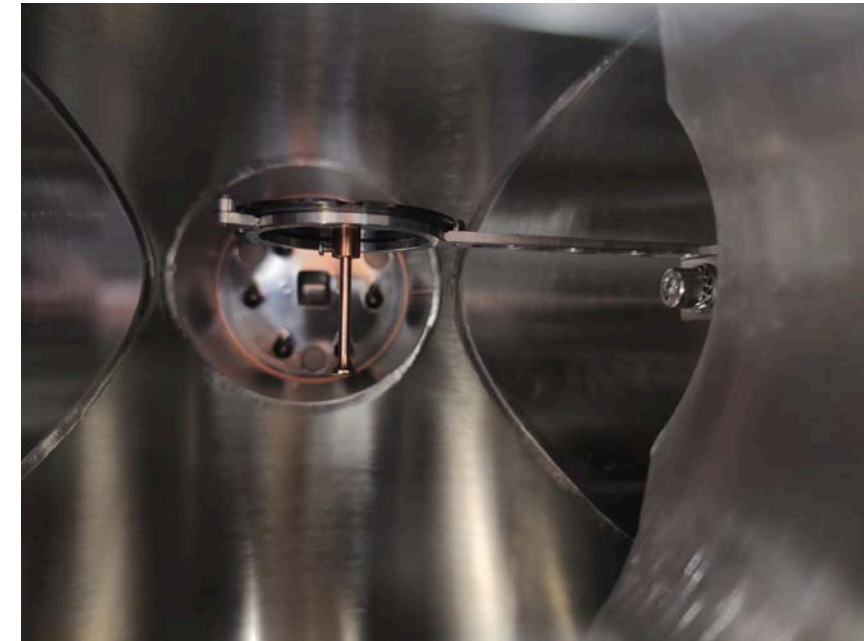
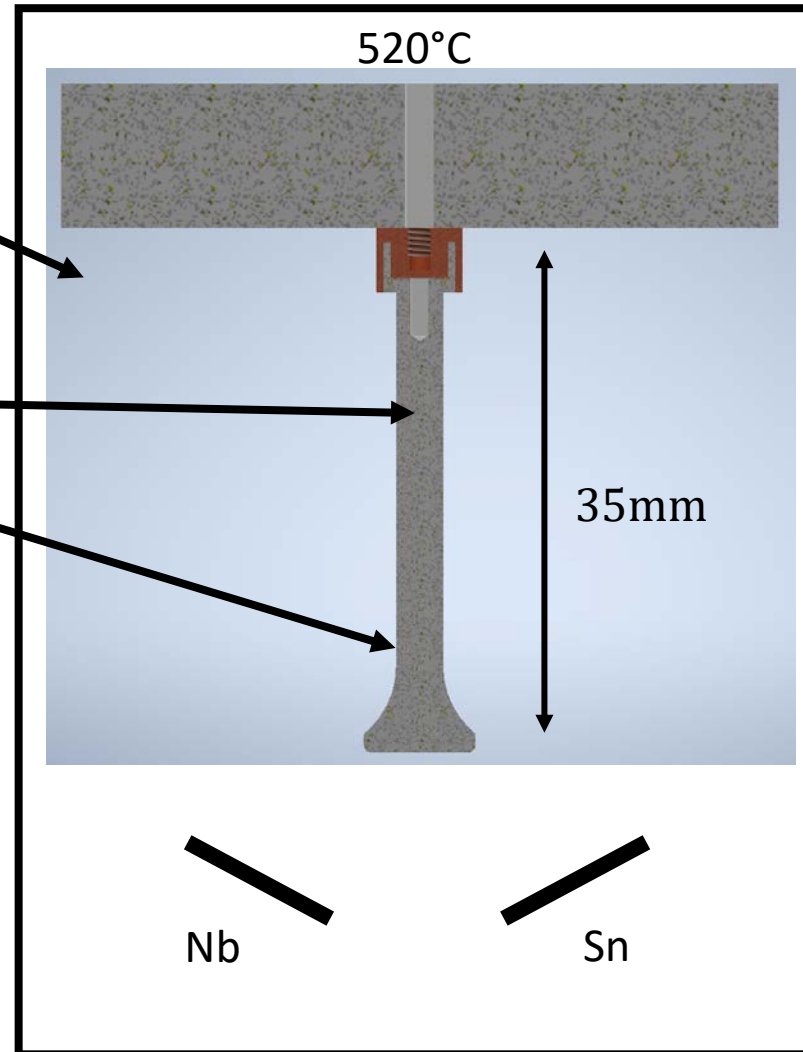
SC THIN FILMS - Nb_3Sn CO-SPUTTERING

Low pressure Ar environment

Cu-antenna
 Nb_3Sn -film

Fixed positions of Nb and Sn source
→ no uniform thickness of the film

Modifications on sample holder are ongoing





DESY Design (right)

- 29.56 mm tip length

Design from RI (left)

- Cyocera feedthrough with flange and antenna tip
- 25 mm tip length

Bakeout at max 300C