



High performance superconductors for next generation particle colliders

Material development and electromechanical studies at UNIGE



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Bruker HTS, Germany

Outline

The FCC dipoles at 16 T: how to get there with Nb₃Sn (LTS)

Reach the ultimate performance:



Investigations on the enhancement of J_c in (Nb,X)₃Sn superconductors by internally oxidized ZrO₂ particles

Withstand the electromagnetic forces:



Electromechanical tests – effects of the transverse stress

Dipole magnets at 20 T and beyond: the call for HTS



Conductor R&D based on YBCO coated conductors for dipole demonstrators

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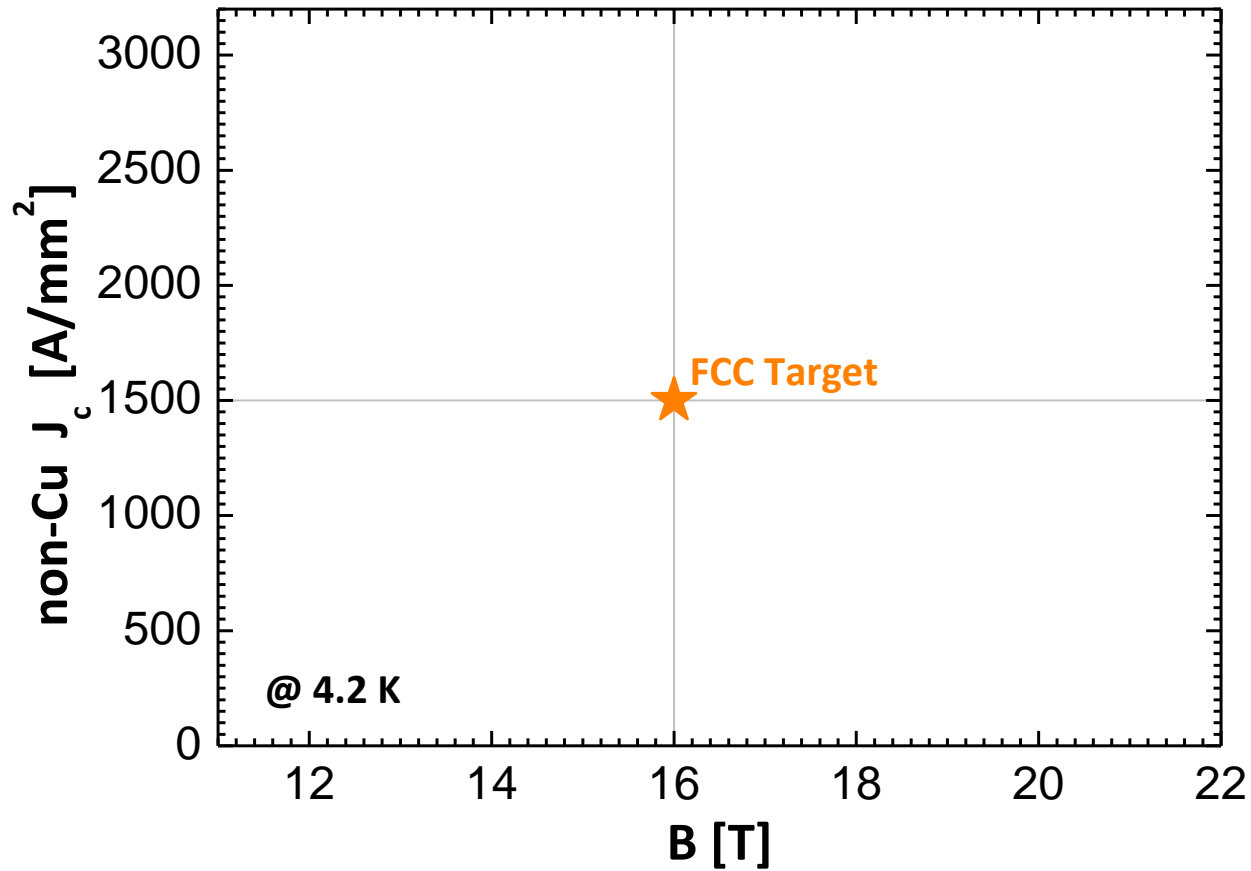
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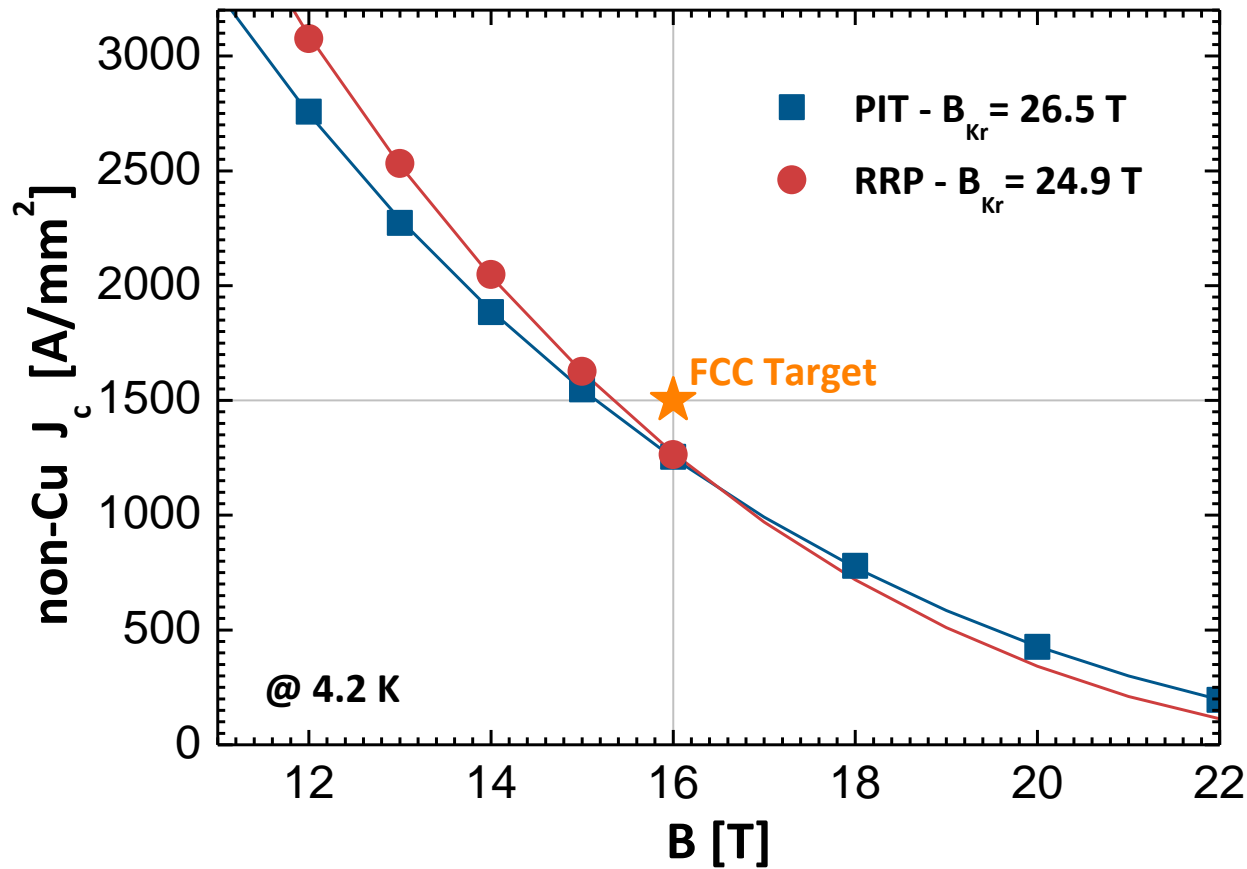


Conductor R&D based on YBCO coated conductors for dipole demonstrators

Performance target non-Cu $J_c(4.2K, 16\text{ T}) = 1500\text{ A/mm}^2$



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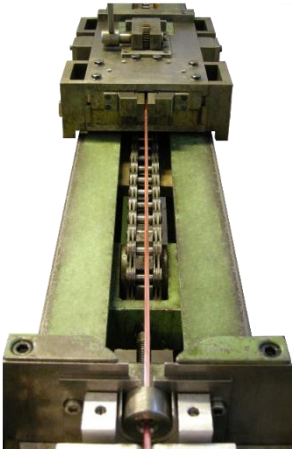


J. Parrell et al., AIP Conf. Proc. 711 (2004) 369

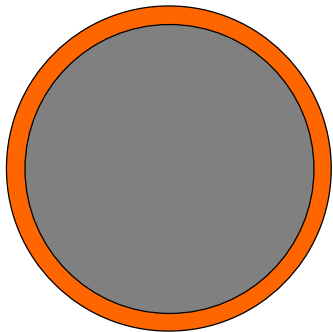
T. Boutboul et al., IEEE TASC 19 (2009) 2564

Equipment and experience in conductor R&D @

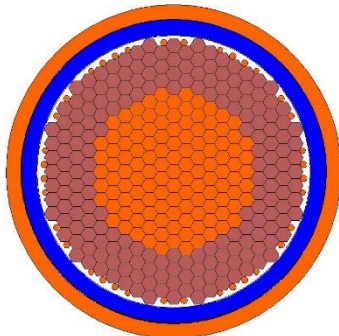
Deformation processes as for industrial production



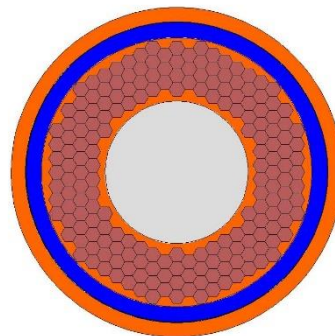
In-house manufacture of multifilamentary conductors



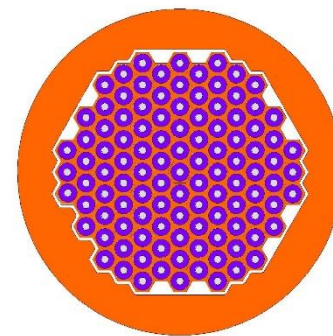
Cu/Nb-Ta rod



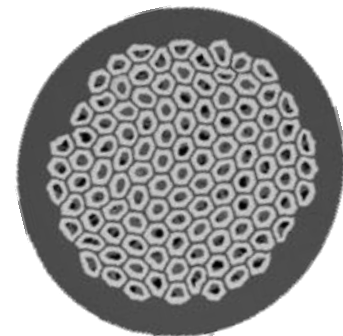
*Sub-element
bundle*



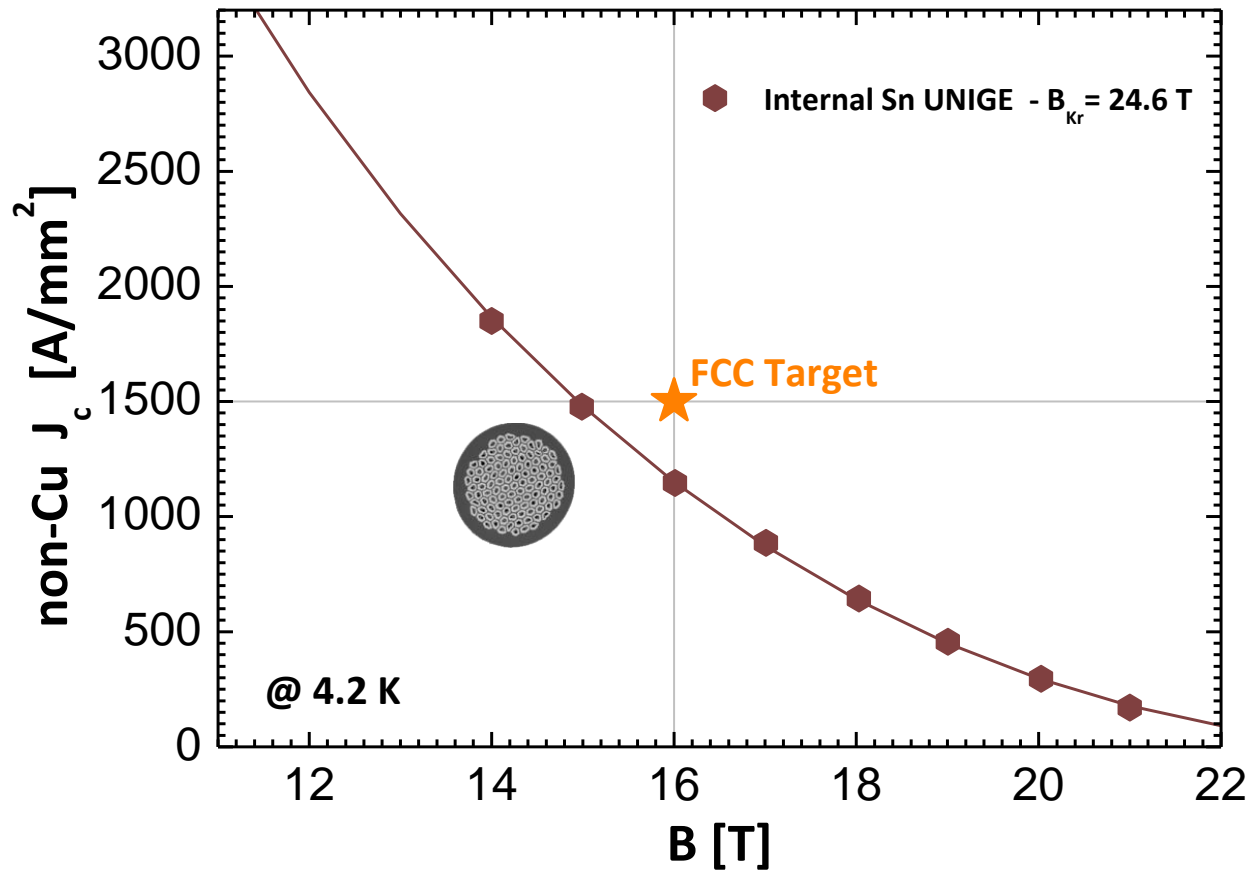
*Sub-element
with pure Sn core*



*Final wire
109 sub-elements*



Performance target non-Cu $J_c(4.2K, 16\text{ T}) = 1500\text{ A/mm}^2$



Grain refinement by Internal Oxidation in Nb_3Sn

Idea from Benz (1968) to form fine precipitates in Nb to impede the Nb_3Sn grain growth

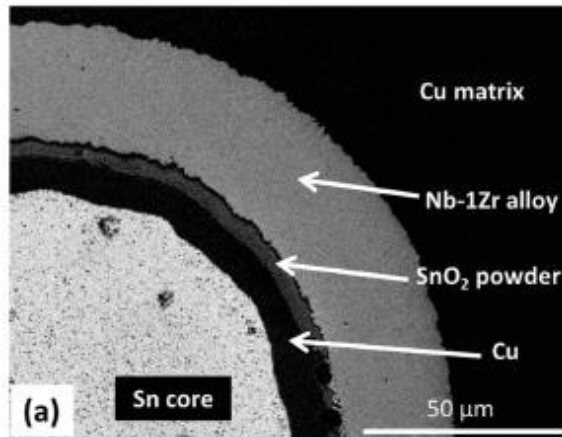
M.G. Benz, Trans. Metall. Soc. AIME, 242 (1968) 1067-1070

Use of a Nb-Zr alloy: Zr has stronger affinity to oxygen than Nb



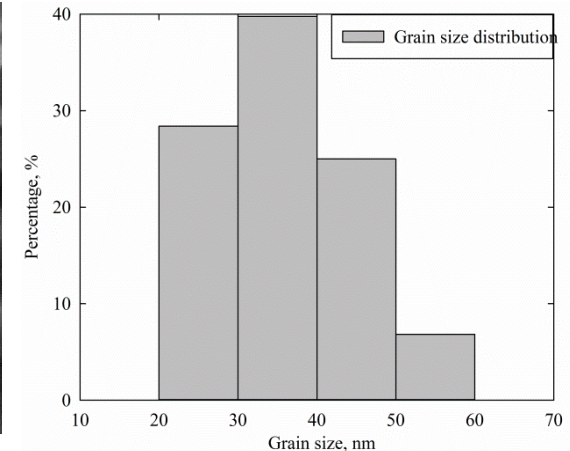
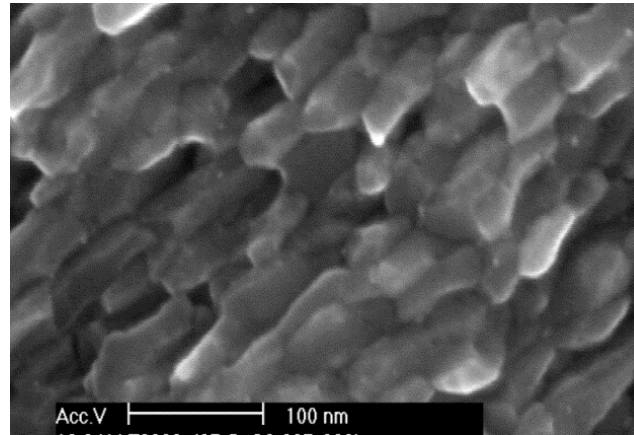
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Oxygen supply added to the composite: oxidation of Zr and formation of nano- ZrO_2



X. Xu et al., APL 104 (2014) 082602

X. Xu et al., Adv. Mat. 27 (2015) 1346



Average grain size is reduced down to ~ 50 nm in binary Nb_3Sn

Recent advances
on Ta-doped Nb_3Sn

48 filaments, Zr addition, grain size 70-80 nm

X. Xu et al., SuST 32 (2019) 02LT01

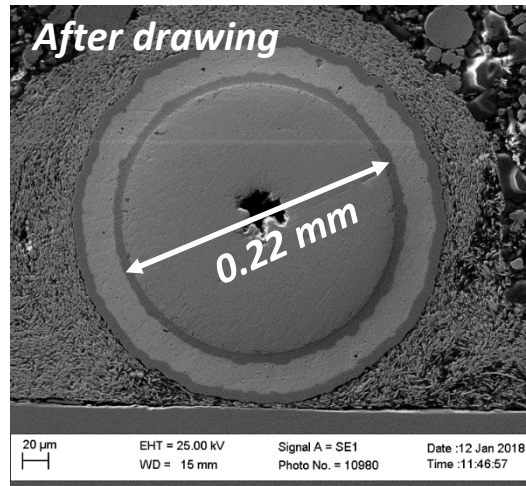
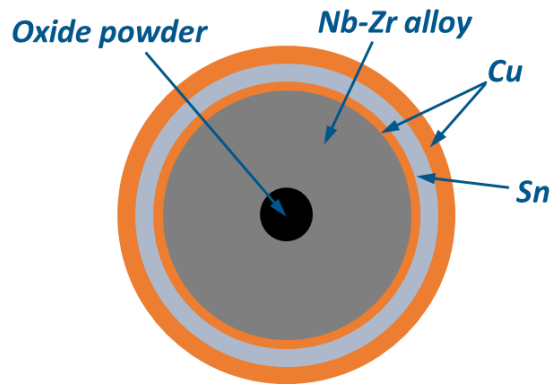
monofilaments, Hf addition, grain size 50-70 nm

S. Balachandran et al., arXiv: 1811.08867 (2018)



Enhancement of J_c in $(Nb,X)_3Sn$ superconductors by internally oxidized ZrO_2 particles

Addendum FCC-GOV-CC-0112 (KE3545/ATS)



Nb alloy	Metal oxide
Nb-7.5wt%Ta	none
Nb-1wt%Zr	MoO ₃
Nb-1wt%Zr	SnO ₂
Nb-1wt%Zr	CuO
Nb-7.5wt%Ta-1wt%Zr	SnO ₂
Nb-7.5wt%Ta-2wt%Zr	SnO ₂

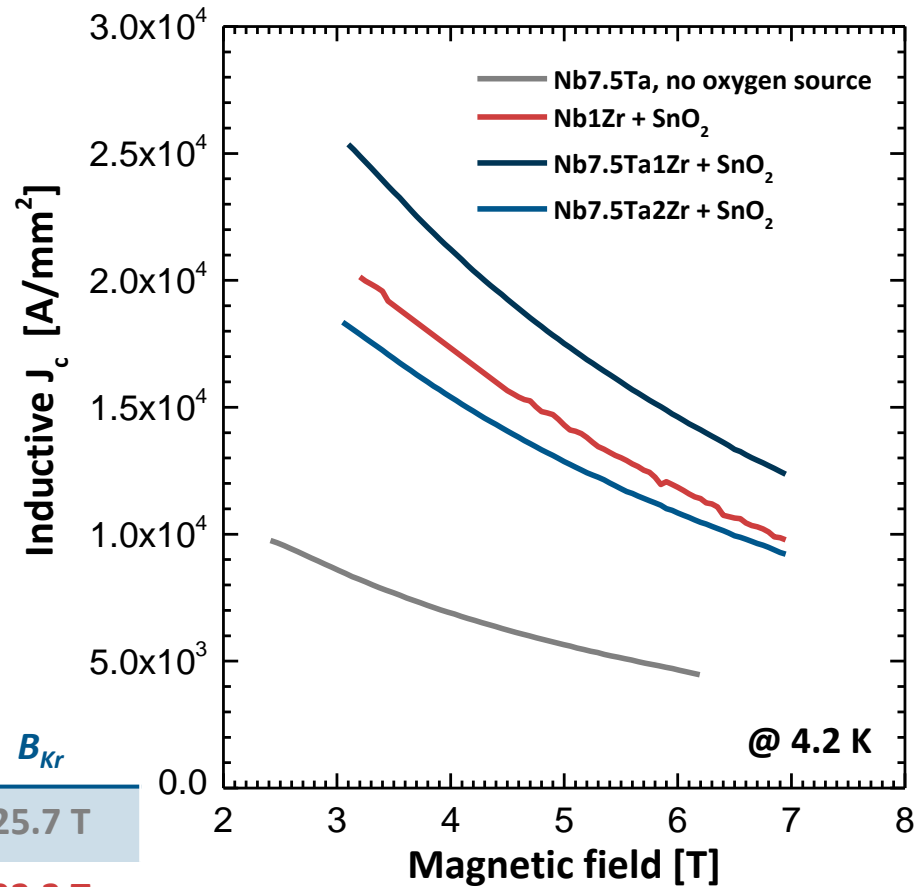
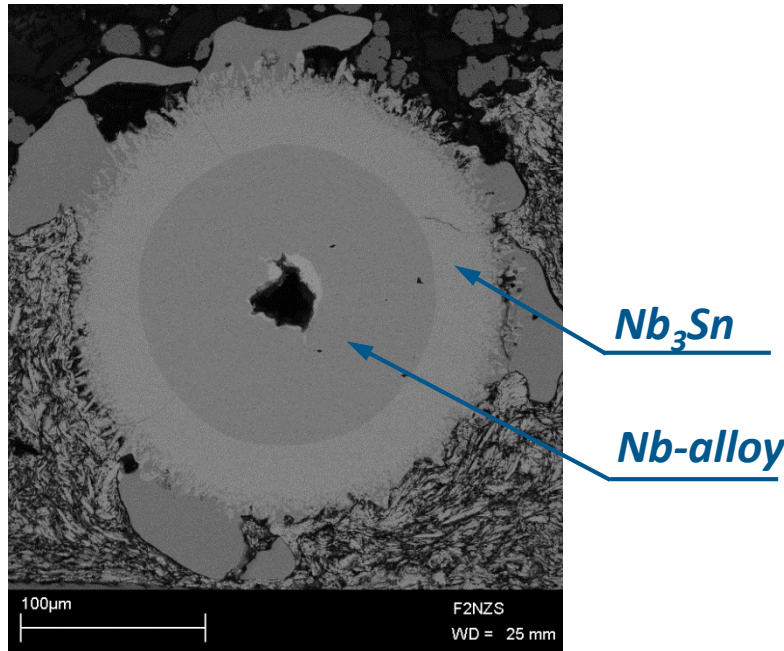
\varnothing 220 μ m wires of Nb alloy were prepared by cold deformation of \varnothing 12 mm rod with nano-sized powders compacted in a central hole

Nb alloy wire was then electroplated successively with: Cu, Sn, Cu

Evaluated different oxygen sources with

- high Gibbs free energy of formation
- low hardness that would make it compatible with wire fabrication
- the metal resulting from the reduction not affecting superconductivity

Results: critical current density



	F_p^{max}	$B @ F_p^{max}$	B_{Kr}
Nb-7.5Ta	28 GN/m ³	5.29 T	25.7 T
Nb-1Zr	71 GN/m ³	5.15 T	22.3 T
Nb-7.5Ta-1Zr	88 GN/m ³	5.45 T	26.6 T
Nb-7.5Ta-2Zr	65 GN/m ³	5.8 T	28.3 T

*One-stage heat treatment @ 650°C/200h
without oxidation step*

*J_c calculated on the entire A15 layer
including fine and large grains*

Results: grain refinement

Median grain size
153 nm

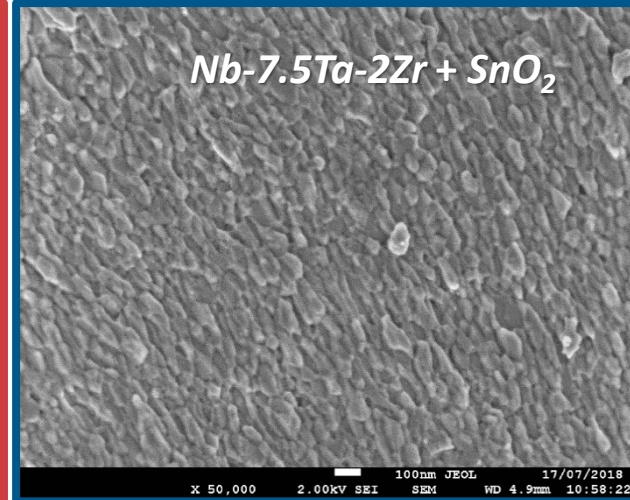
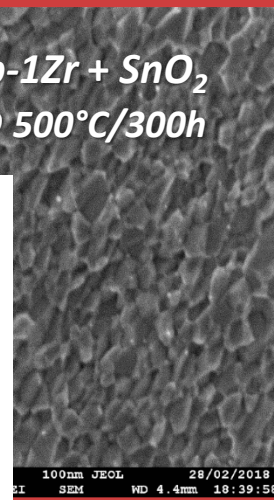
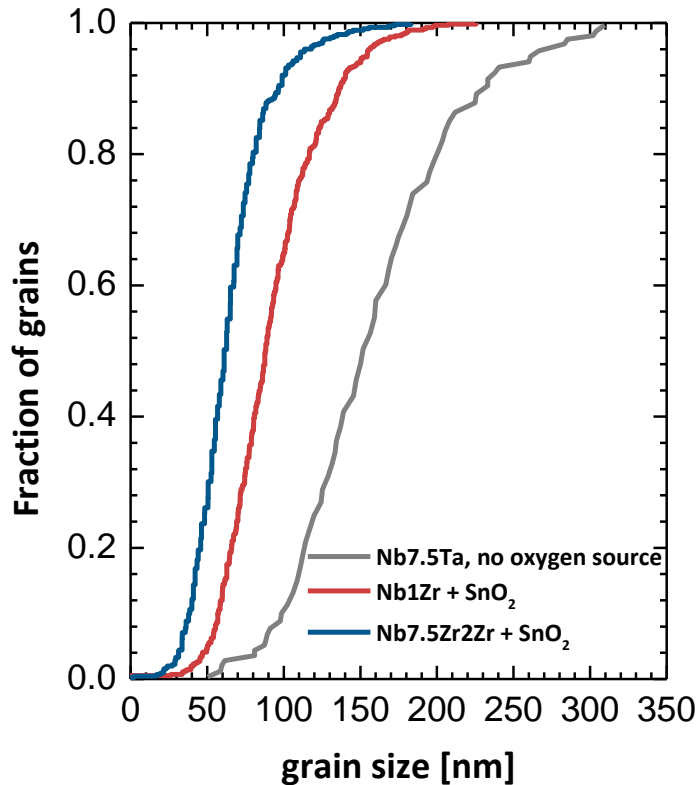
Median grain size
88 nm

Median grain size
61 nm

Nb-7.5Ta Reference

*Nb-1Zr + SnO₂
Oxidation @ 500°C/300h*

Nb-7.5Ta-2Zr + SnO₂



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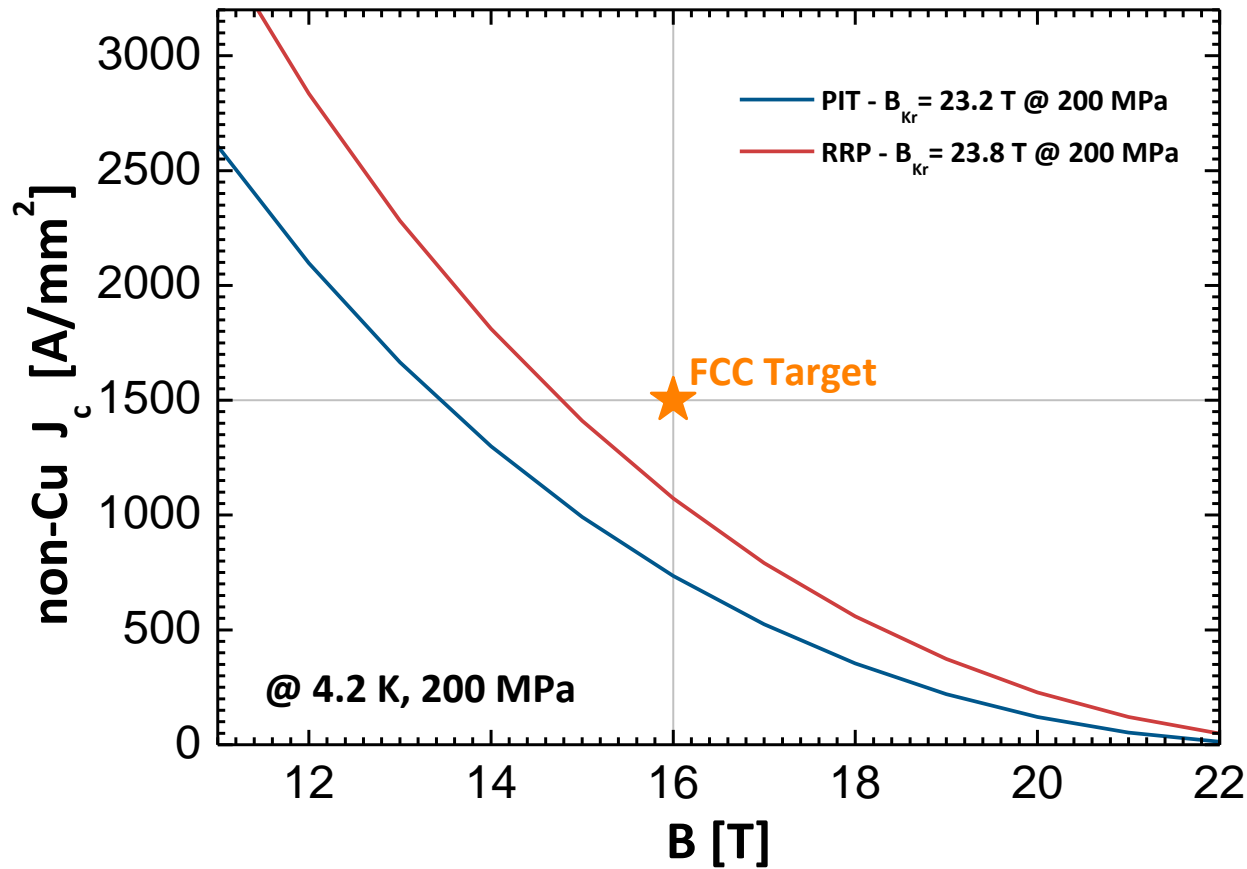
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Conductor R&D based on YBCO coated conductors for dipole demonstrators

**Performance target non-Cu $J_c(4.2K, 16 T) = 1500 A/mm^2$
and 200 MPa**



J. Parrell et al., AIP Conf. Proc. 711 (2004) 369

T. Boutboul et al., IEEE TASC 19 (2009) 2564

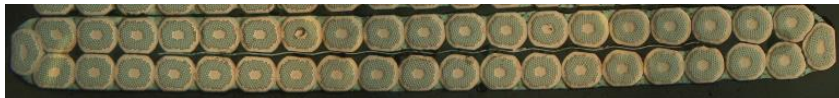


Stress limits for the design of the 16 T dipoles for the Future Circular Collider

H2020 EuroCirCol WP5 Task 5: Conductor studies

*The 16 T FCC dipoles are being designed with a **peak stress of 150-200 MPa** at operation*

Are the Nb_3Sn wires in the cable able to withstand such a high stress level? Which degradation is tolerable?

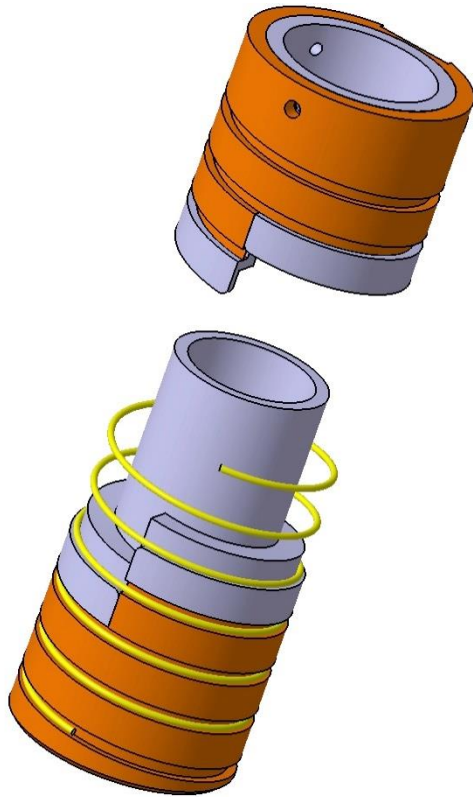


Nb_3Sn Rutherford cable for HL-LHC, 40 strands

- *Nb_3Sn wires are deformed during cabling*
- *Cables are braided with glass fiber*
- *The winding is impregnated with resin*

*Is it possible to extrapolate the **behaviour of the cable** from a **single wire experiment**?*

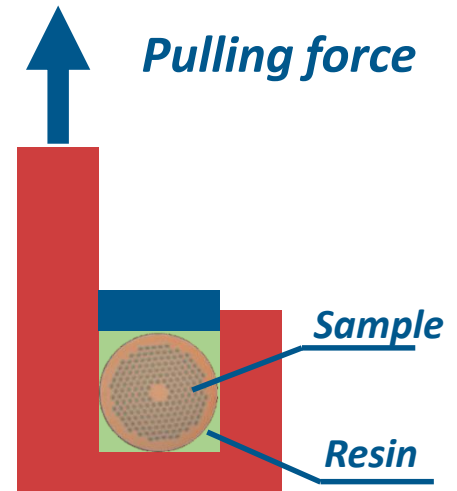
The WASP concept for I_c vs. transverse stress



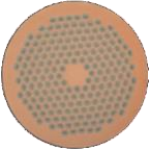
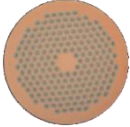



B. Seeber et al., IEEE TASC 17 (2007) 2643

G. Mondonico et al., SUST 25 (2012) 115002

4-WALL + impregnation

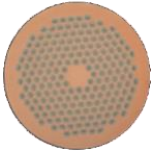
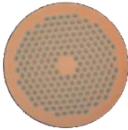


Measurement campaign on high- J_c Nb_3Sn wires

	Technology	# of subelements	Diameter [mm]	Wire ID
	PIT	192	1.0	#0904 #31712 #14310
	PIT	192	0.85	#29992
	RRP	108/127	0.85	#14753 #14516 (Ta) #76A08U
	RRP	132/169	1.0	#15114 #114163
	RRP	132/169	0.85	#14393

Cu/non Cu ratio between 1.2 and 1.3 for all wires

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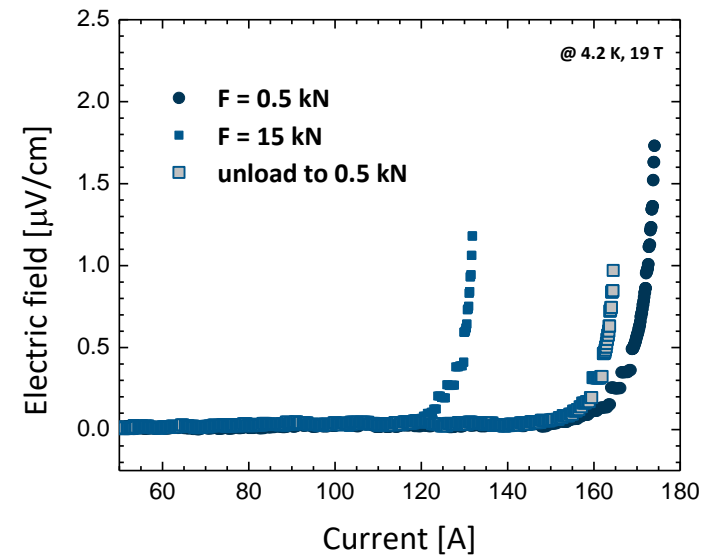
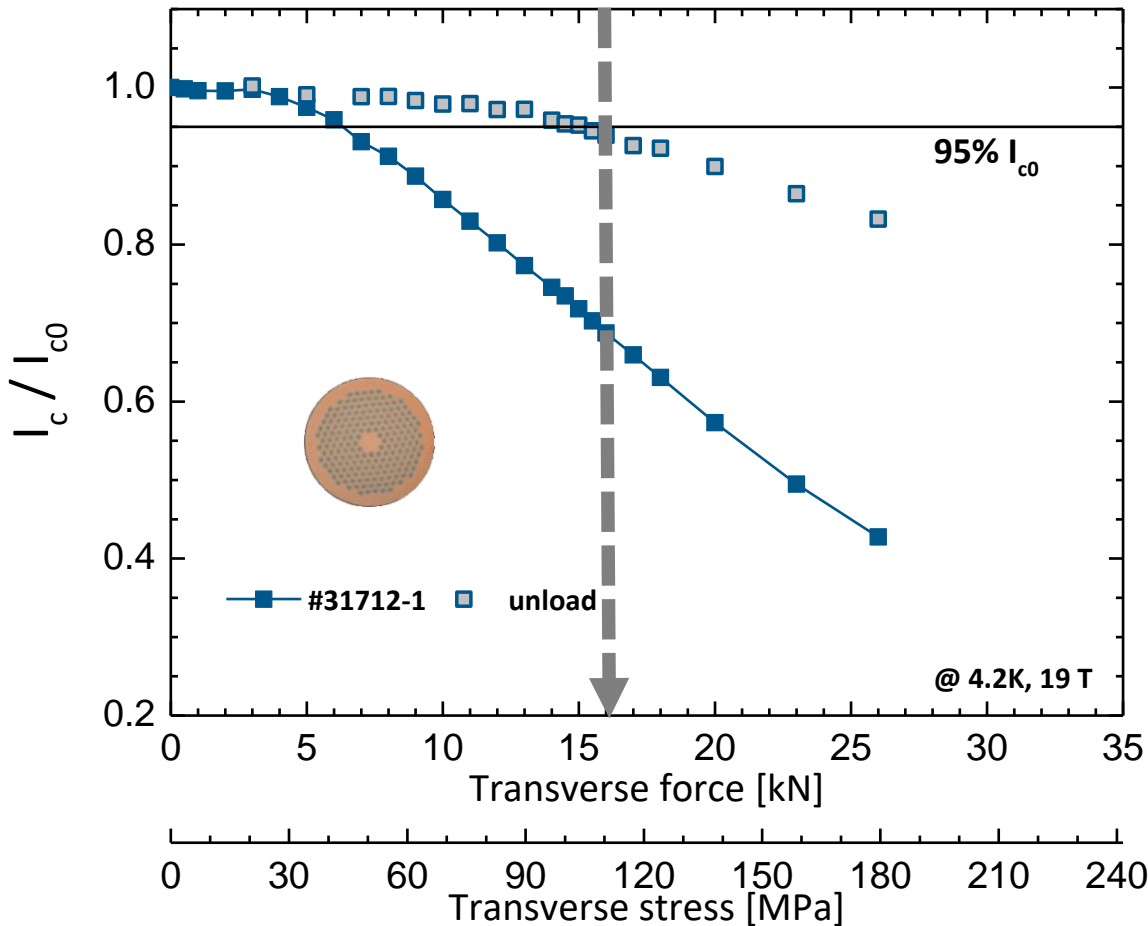
Impact of the impregnation type on the irreversible stress limits

Tests performed with

- Epoxy L — About the same elastic modulus as CDT 101K
- Glass fiber sleeve + Epoxy L
- Stycast — ~ 2x elastic modulus of CDT 101K

I_c vs. transverse stress

PIT 192 + epoxy L



The irreversible limit is defined at the force level leading to a 95% recovery of the initial I_c after unload

Here

$$F_{irr}(B=19\text{T}) = 16 \text{ kN}$$

The corresponding irreversible stress limit is

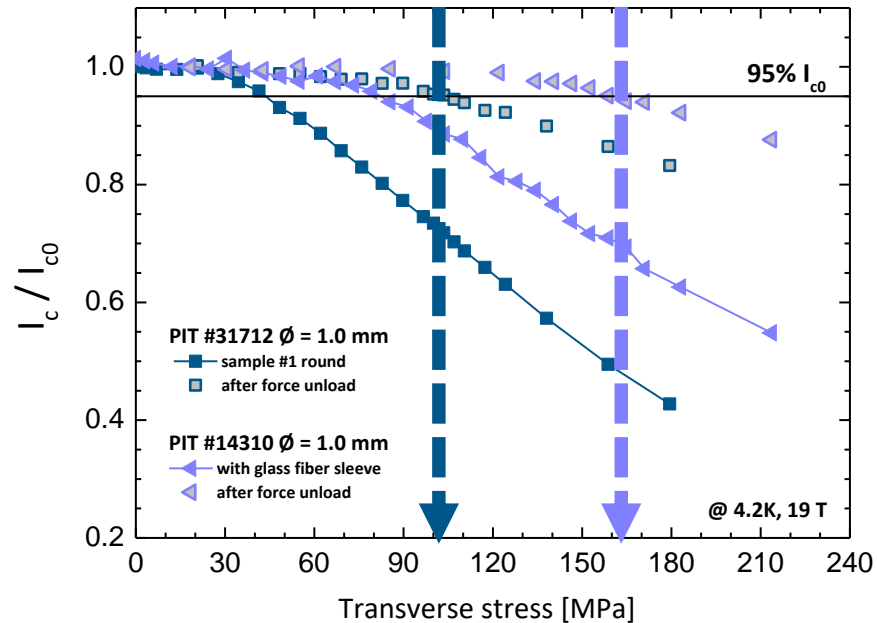
$$\sigma_{irr}(B=19\text{T}) = 110 \text{ MPa}$$

where

$$\text{Stress} = \frac{\text{Force}}{\text{groove length} \times \text{groove width}}$$

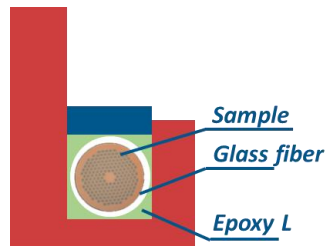
Reinforced impregnation

wire in a glass fiber sleeve + Epoxy L

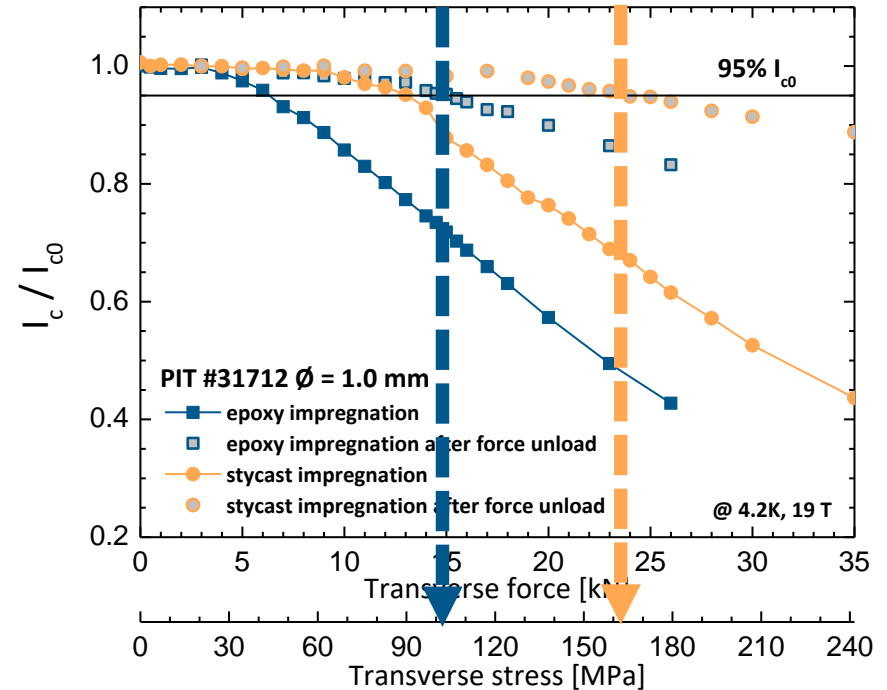


Epoxy L $\rightarrow \sigma_{irr}(B=19T) = 110$ MPa

Glass fiber sleeve + Epoxy L $\rightarrow \sigma_{irr}(B=19T) = 165$ MPa








wire + Stycast



Epoxy L $\rightarrow \sigma_{irr}(B=19T) = 110$ MPa

Stycast $\rightarrow \sigma_{irr}(B=19T) = 162$ MPa

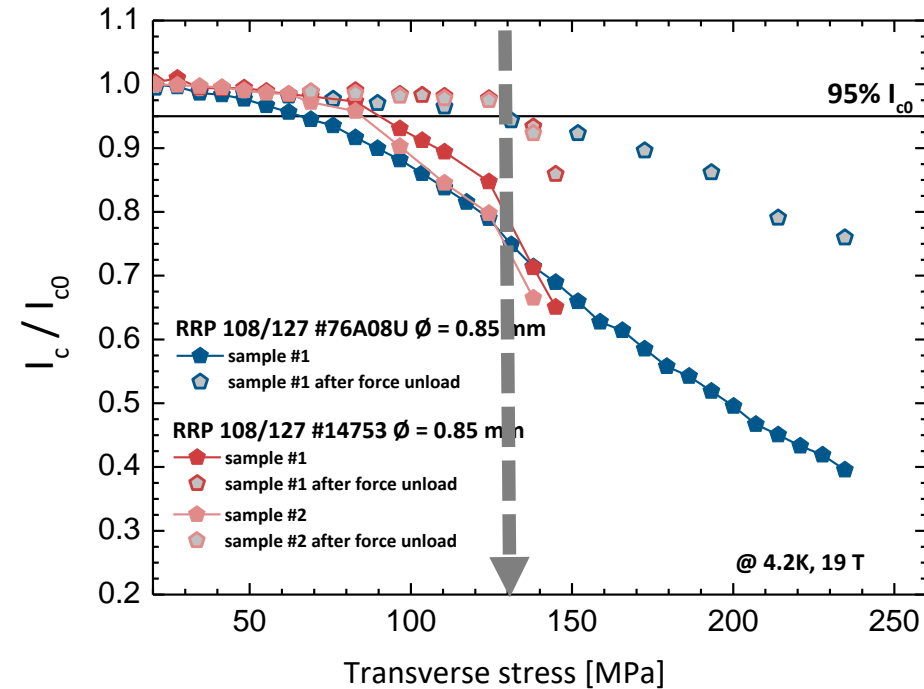
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		<i>Technology</i>	<i># of subelements</i>	<i>Diameter [mm]</i>	<i>Wire ID</i>
		<i>RRP</i>	<i>108/127</i>	<i>0.85</i>	<i>#14753 #14516 (Ta) #76A08U</i>
		<i>RRP</i>	<i>132/169</i>	<i>1.0</i>	<i>#15114 #114163</i>
		<i>RRP</i>	<i>132/169</i>	<i>0.85</i>	<i>#14393</i>

Impact of the wire layout on the irreversible stress limits

All tests performed with Epoxy L impregnation

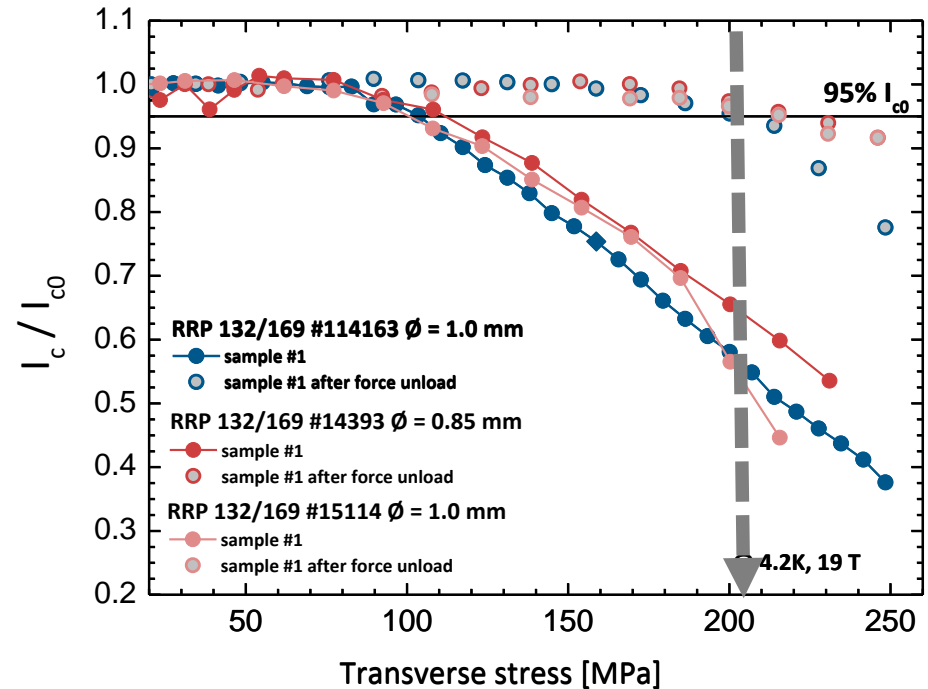
RRP: 108/127 vs. 132/169



RRP 108/127



Irreversible stress limit ~ 130 MPa at 19 T



RRP 132/169



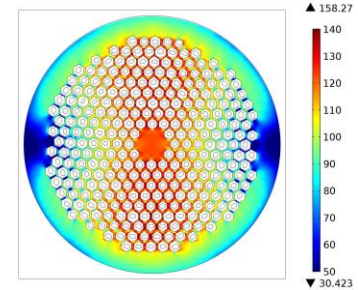
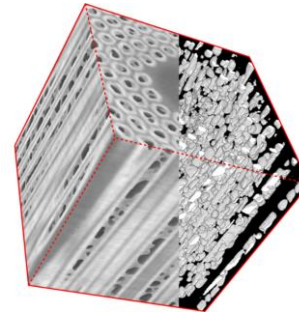
Irreversible stress limit ~ 200 MPa at 19 T

Better stress redistribution in RRP 132/169, likely due to the arrangement and to the smaller relative diameter of the subelements

Other effects under investigation

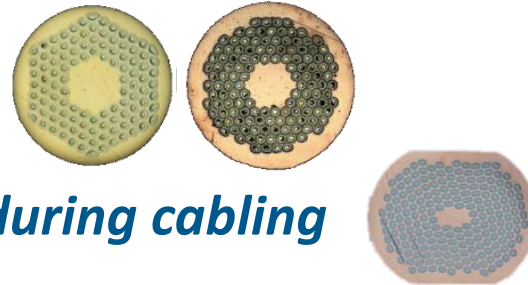
Mechanisms responsible of the irreversible degradation of the critical current

- *plastic deformation and residual stress vs. filament cracks*
- *stress concentration at voids*



Redistribution of the applied stress

- *effects of the filament layout*
- *effects of the wire deformation during cabling*



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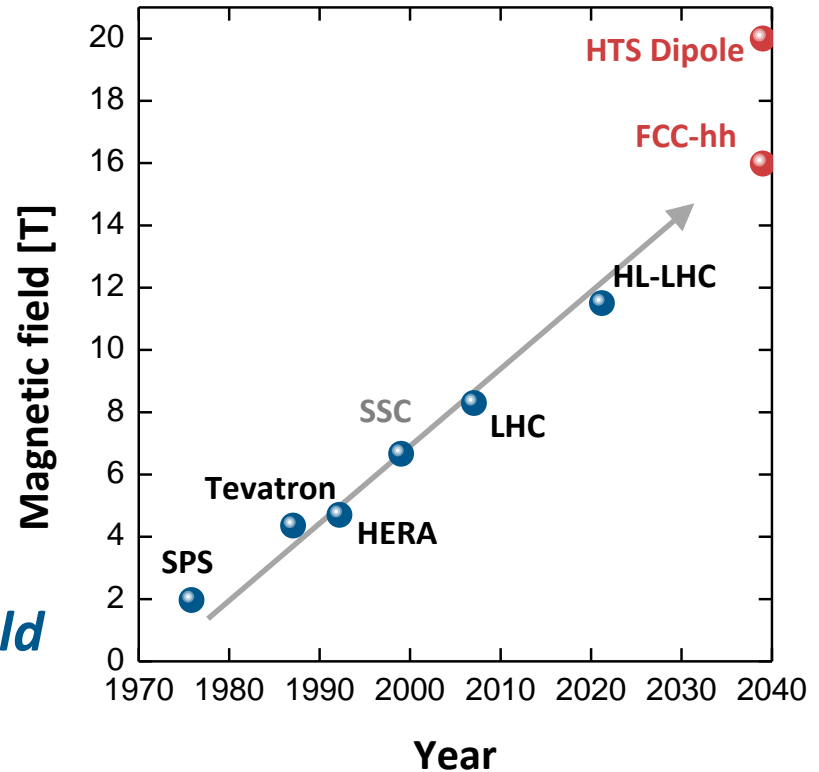
Setting the scene

The goal of 20 T in an accelerator quality dipole calls for HTS

 *EuCARD² has developed*

- *a HTS CONDUCTOR for accelerator dipoles (10 kA-class cable)*
- *a DIPOLE DEMONSTRATOR with accelerator quality (5 T, 40 mm bore)*

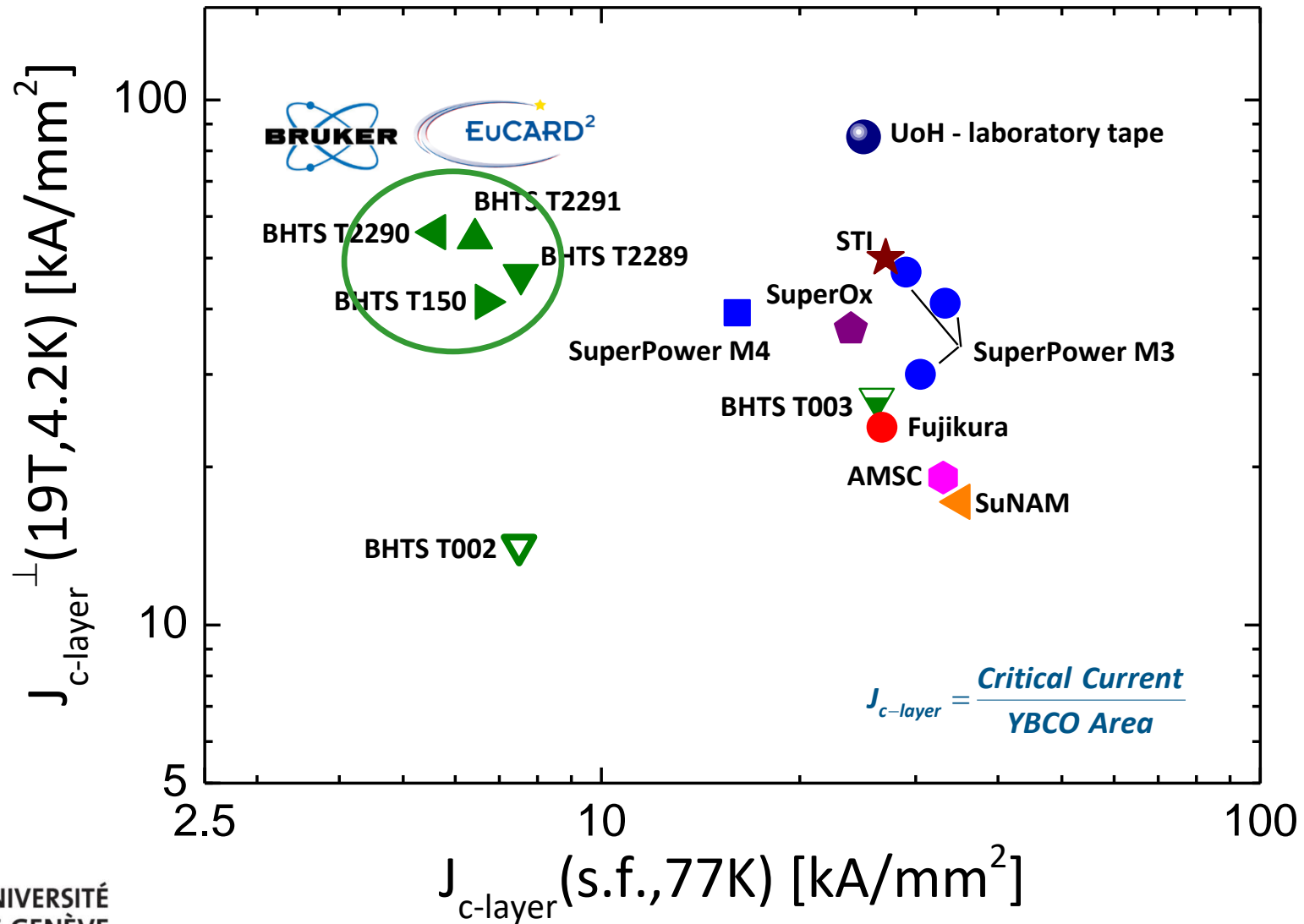
Tests of the coils as stand alone and in-field are ongoing



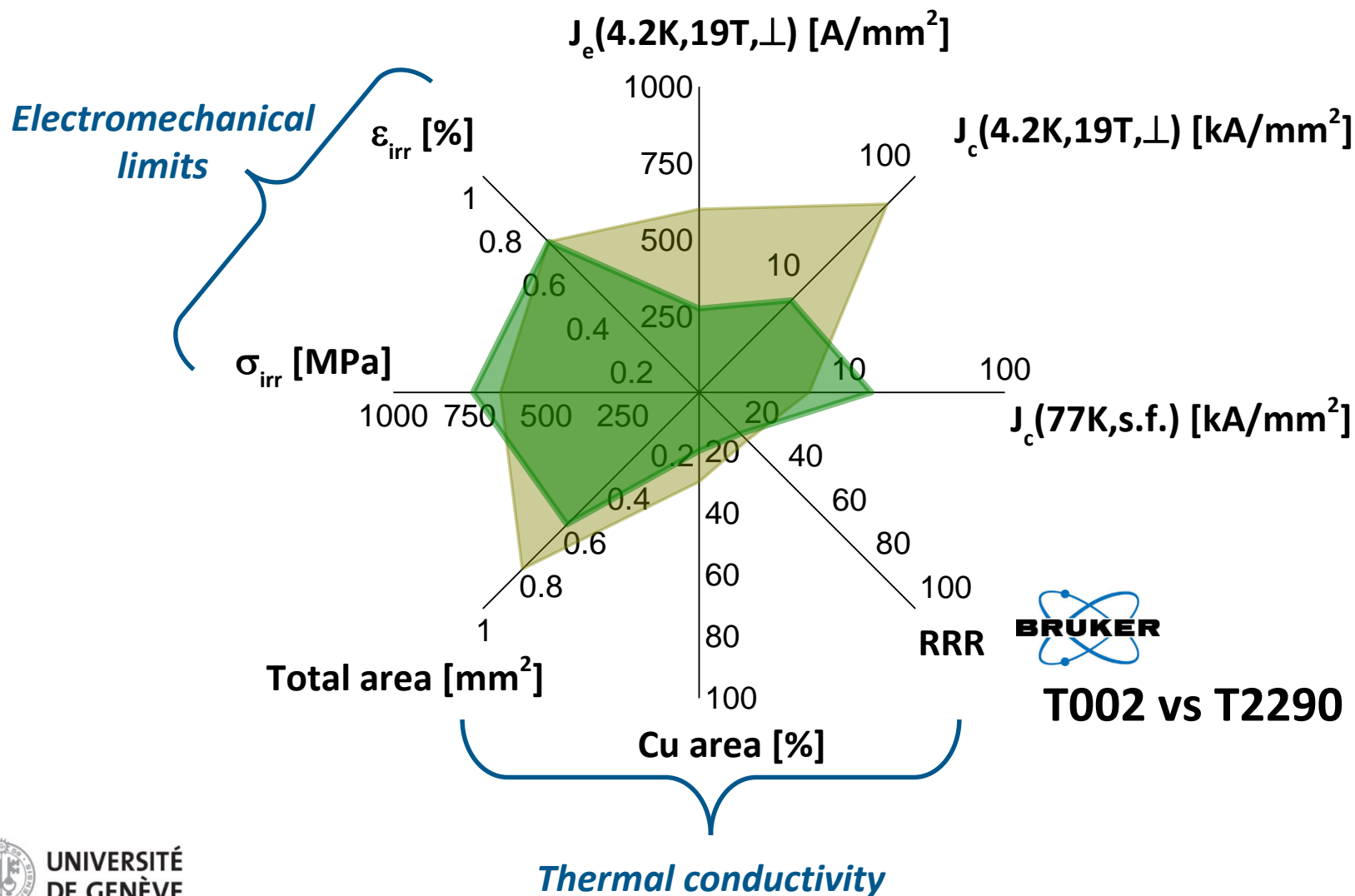
 *ARIES is building on the shoulders of* 

Performance overview: $J_c(s.f., 77K)$ vs. $J_c^\perp(19T, 4.2K)$

(Data from 2016)

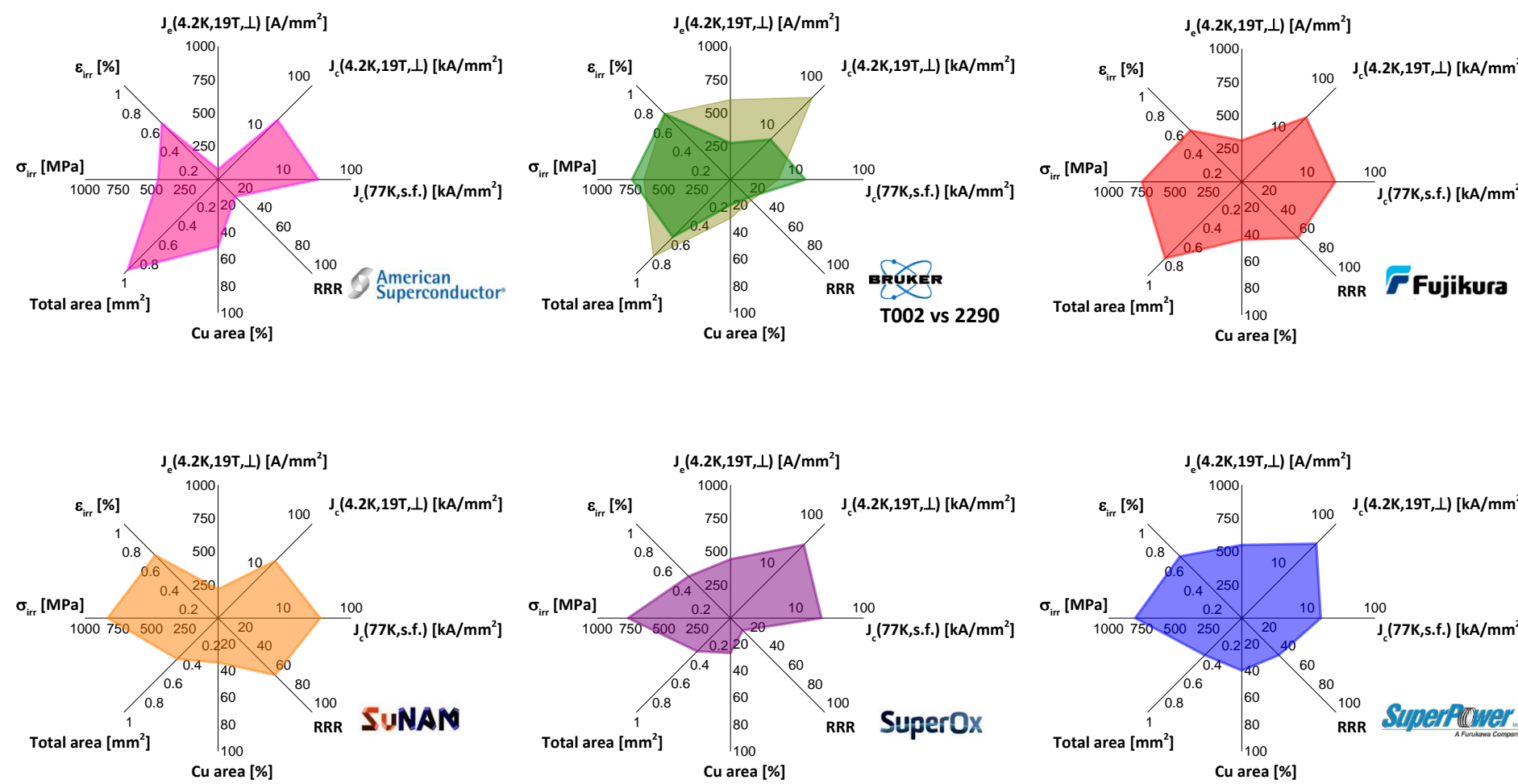


Is high J_c all you need ?

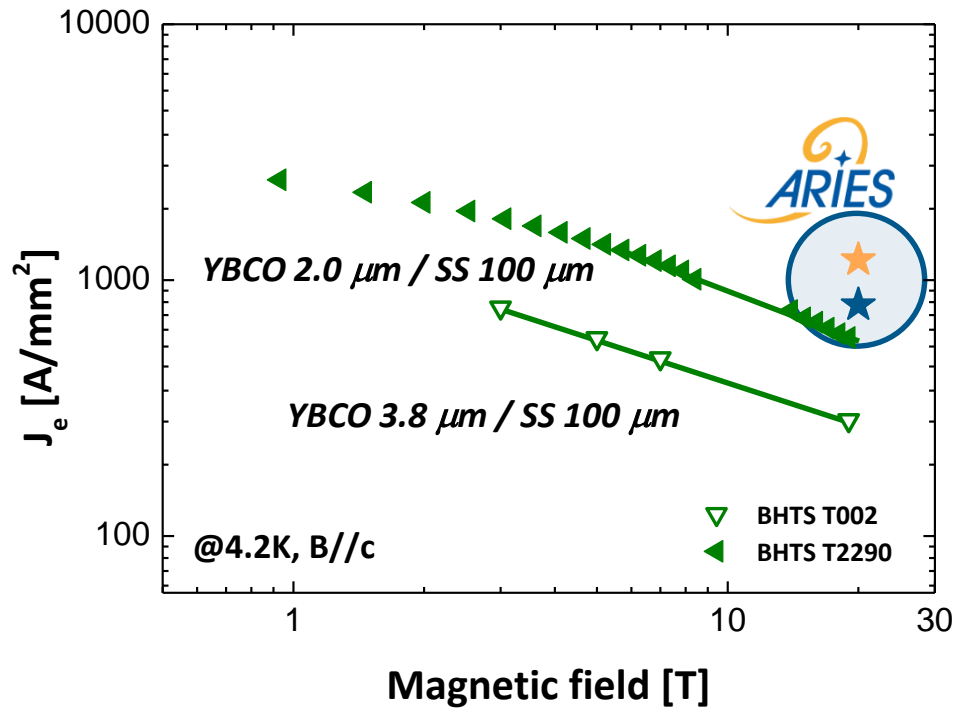


Main parameters at a glance

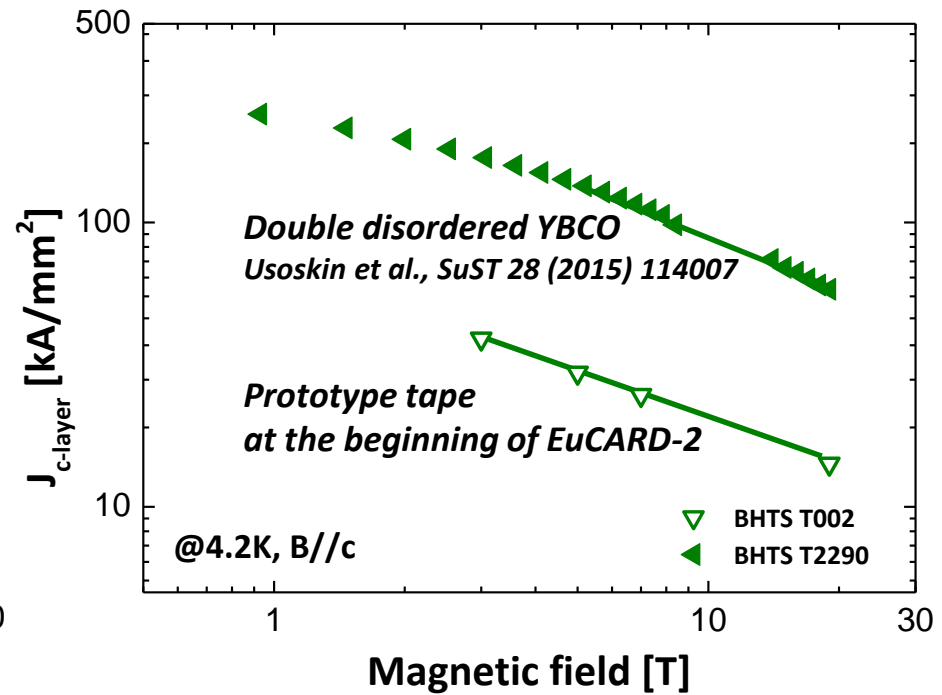
(Data from 2016)



Performance target for **ARIES**: $J_e(4K, 20T) = 800-1200 \text{ A/mm}^2$

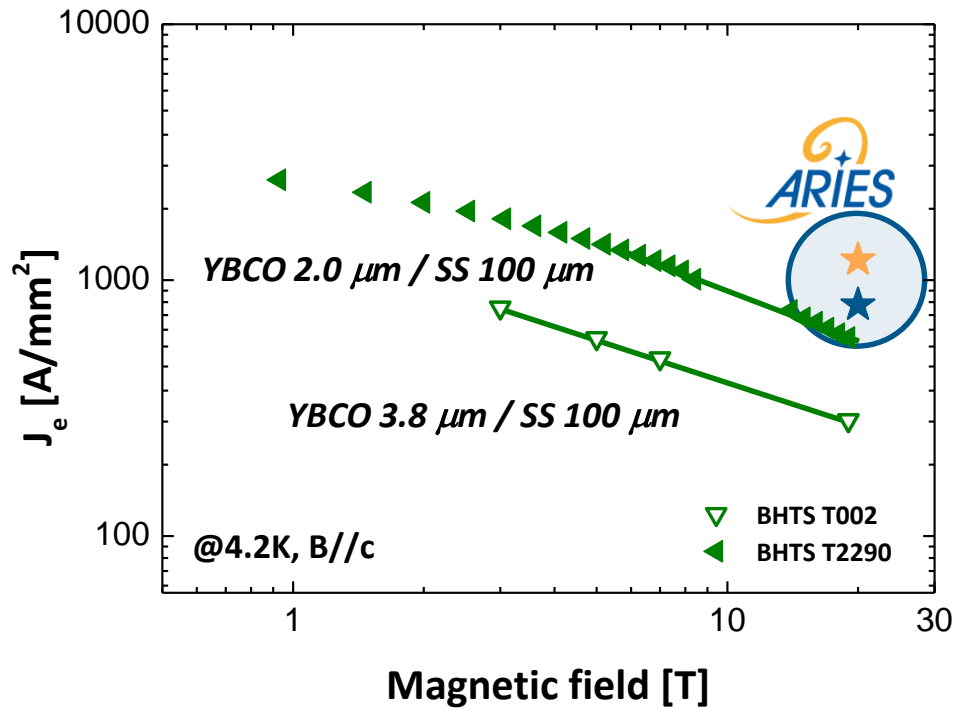


$$J_e = \frac{\text{Critical Current}}{\text{Total Area}}$$



$$J_{c\text{-layer}} = \frac{\text{Critical Current}}{\text{YBCO Area}}$$

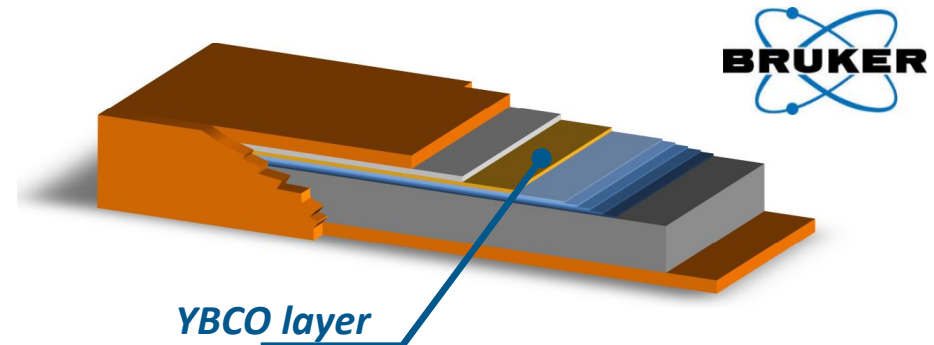
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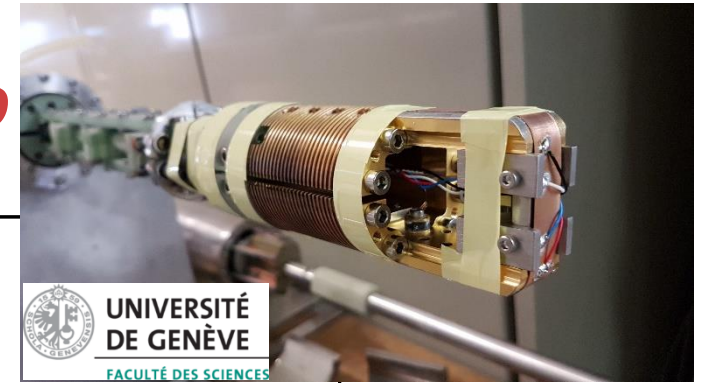
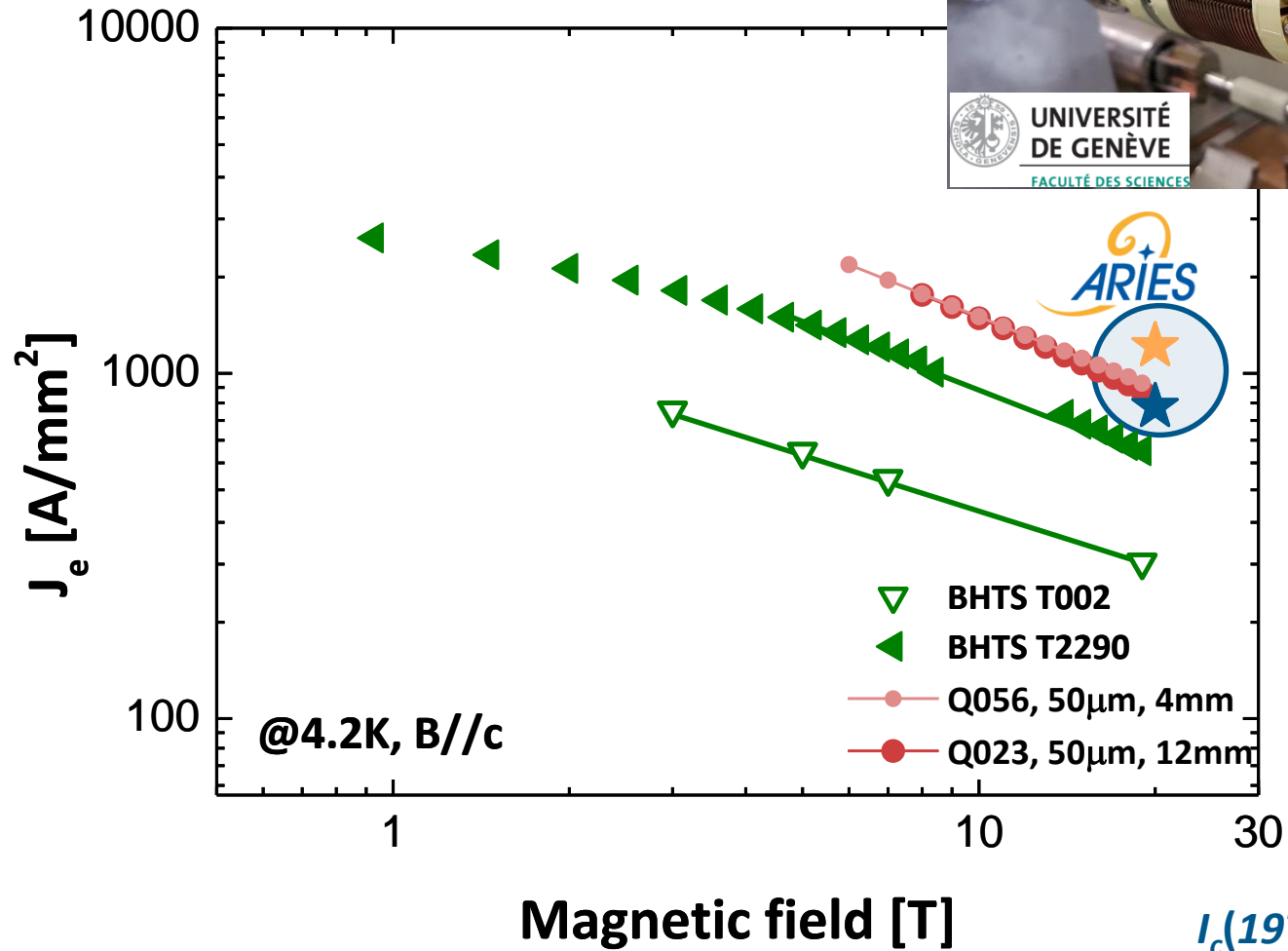
How to get there?

- Increase the layer J_c of YBCO
- Increase the thickness of YBCO
- Reduce the thickness of the substrate **100 μm SS \rightarrow 50 μm SS**

$$J_e = \frac{\text{Critical Current}}{\text{Total Area}}$$



First I_c measurements: where do



	$I_c(19T)$	$J_e(19T)$
12 mm	957 A	886 A/m ²
4 mm	337 A	936 A/m ²

Summary

Driving Nb₃Sn towards its ultimate performance

- *produced material with refined grains and high B_{Kr}*
- *further optimization of the process is ongoing*

Exploring the intrinsic and extrinsic effects behind the irreversible degradation of I_c under transverse stress

- *tested different impregnations and load configurations: resins with higher rigidity perform better*
- *RRP wires are less sensitive to transverse loads than PIT wires*

Improving the performance of YBCO coated conductors for applications to HEP magnets

- *obtained a record $J_e > 900 \text{ A/mm}^2$ @ 4.2 K, 19 T*

Thank you for the attention !

Carmine SENATORE

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<http://supra.unige.ch>