

**23 January 2019**

# Saito Kazuyoshi

# Japan Superconductor Technology, Inc.

Workshop on advanced superconducting  
materials and magnet  
@ KEK, Japan 23<sup>rd</sup> Jan. 2019

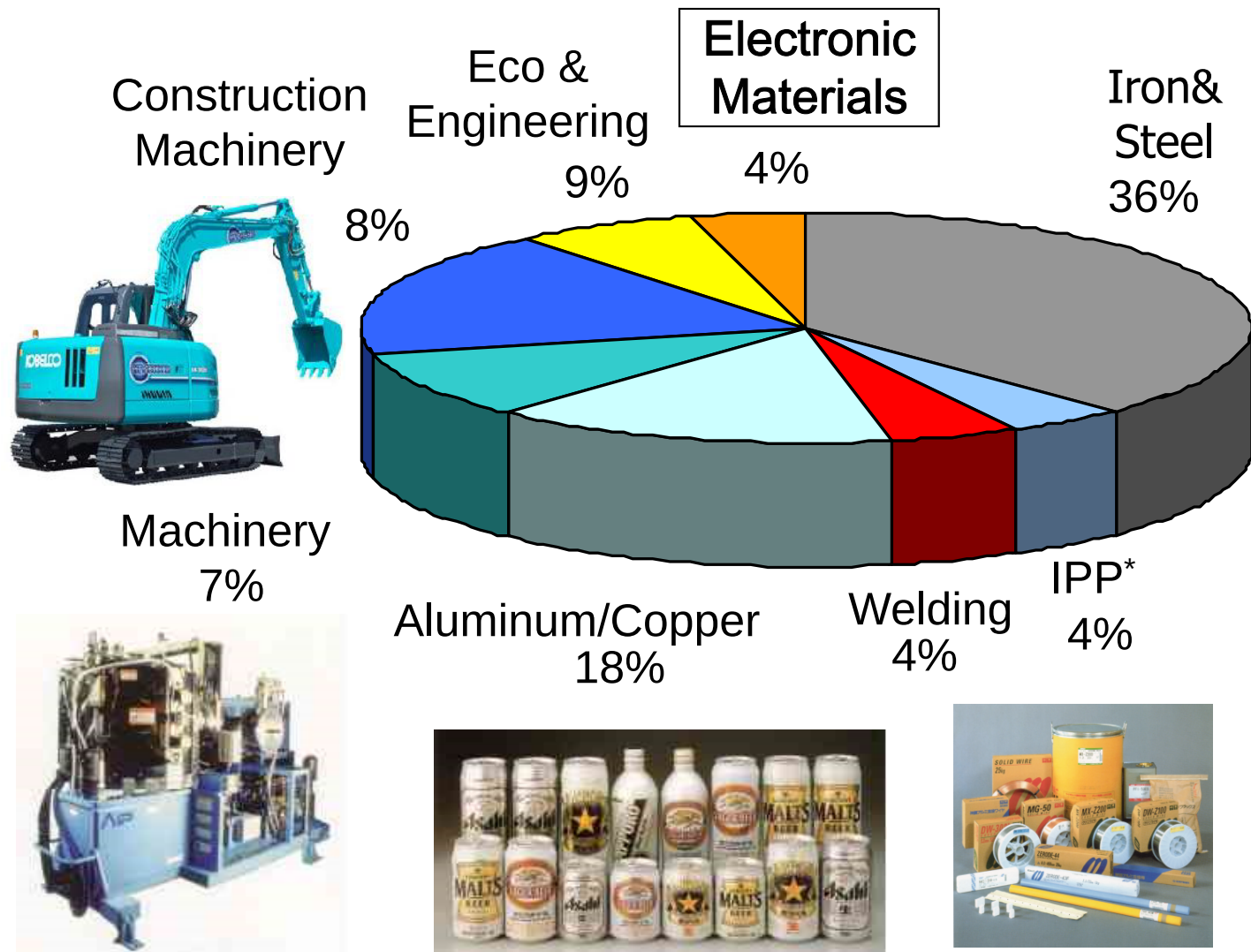
# Today's OUTLINE

- 1) About JASTEC
- 2) Nb<sub>3</sub>Sn wire for NMR magnet
- 3) Nb<sub>3</sub>Sn wire for ITER
- 4) Nb<sub>3</sub>Sn wire for FCC

# About JASTEC

# Outline of Kobe Steel Group (FY 2017)

Consolidated Net Sales : US\$ 17.1 billion



IPP:  
Independent  
Power  
Producer



# Company Profile

Export to  
Overseas Customers

**Founded** : Apr. 1<sup>st</sup>, 2002  
**Capital** : 400 mil JP Yen  
**Shareholder** : Kobe Steel (100%)  
**Employee** : 169 (Dec. 2018)  
**President** : Dr. T. Miyatake



Eco-action 21

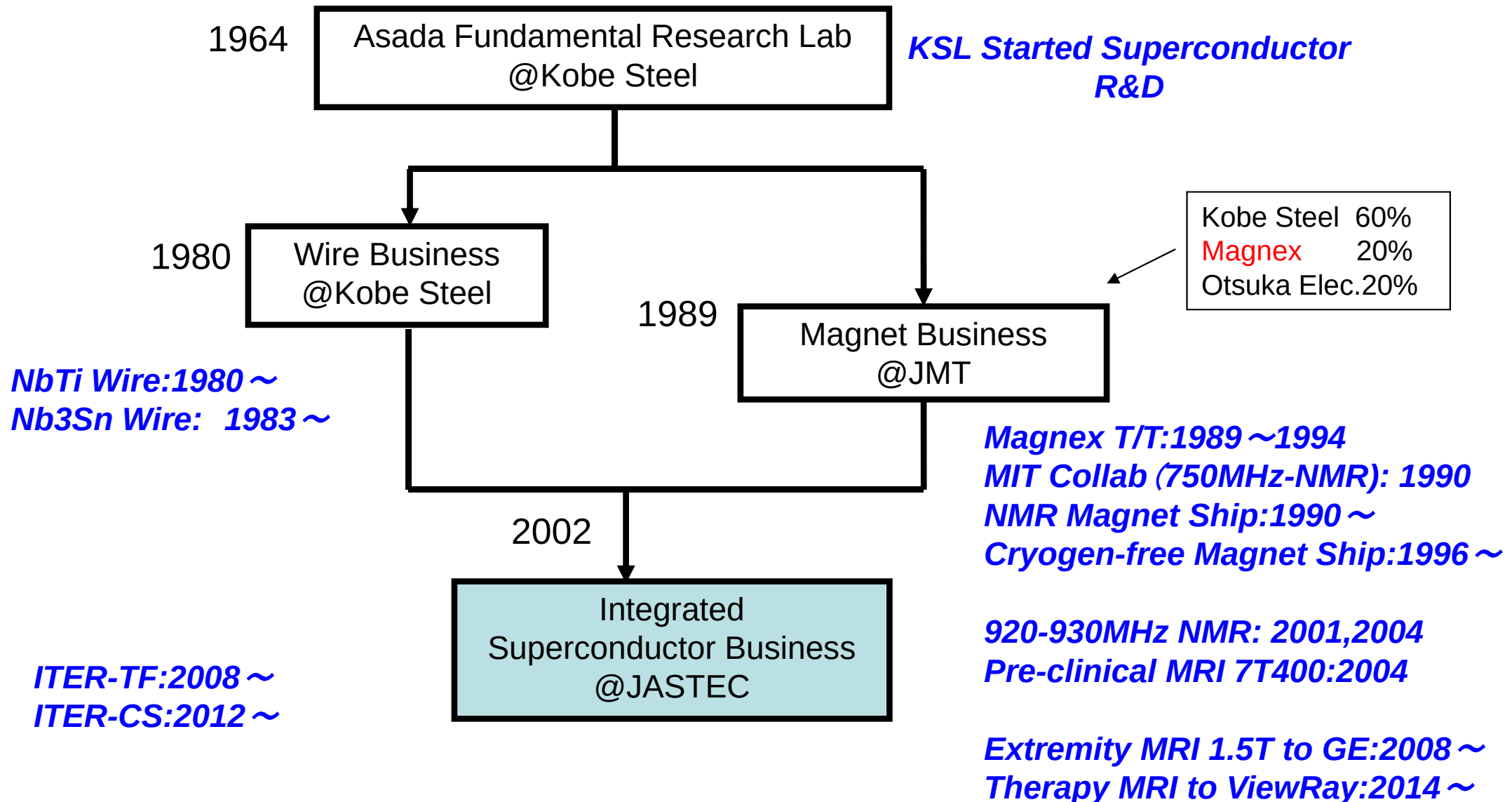
**TOKYO  
Sales**

**KOBE  
Head office  
Magnet factory**

**MOJI  
Wire factory**



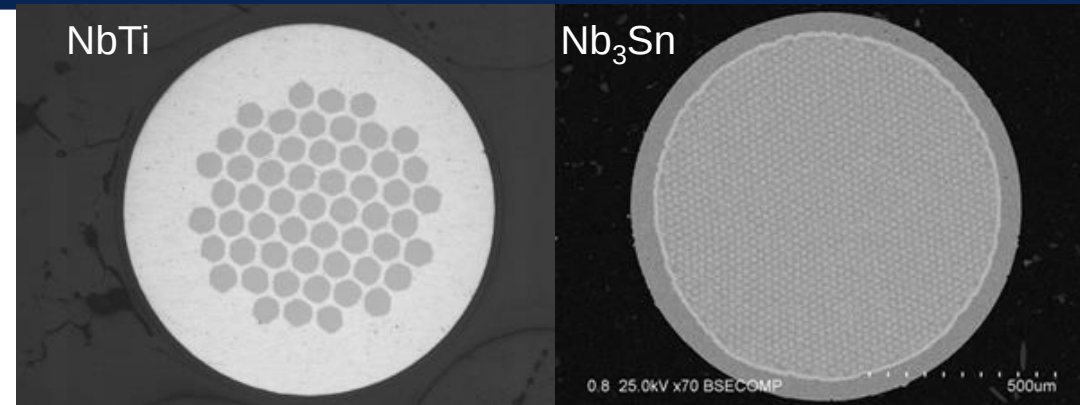
# Company history



# Current products lineup in JASTEC

## Superconducting wire

- ✓ NbTi  $\Rightarrow$  low magnetic field
- ✓ Nb<sub>3</sub>Sn  $\Rightarrow$  high magnetic field



## Superconducting magnet

- ✓ Biology/Chemical Analysis : NMR
- ✓ Medical Imaging : MRI
- ✓ Silicon Crystal Growth : MCZ
- ✓ Gyrotron: High power Microwave radiation



# High performance Nb<sub>3</sub>Sn wire development in JASTEC/KSL

## ◆ NMR magnet

Filed :18T

200-300A/mm<sup>2</sup>

## ◆ ITER coils

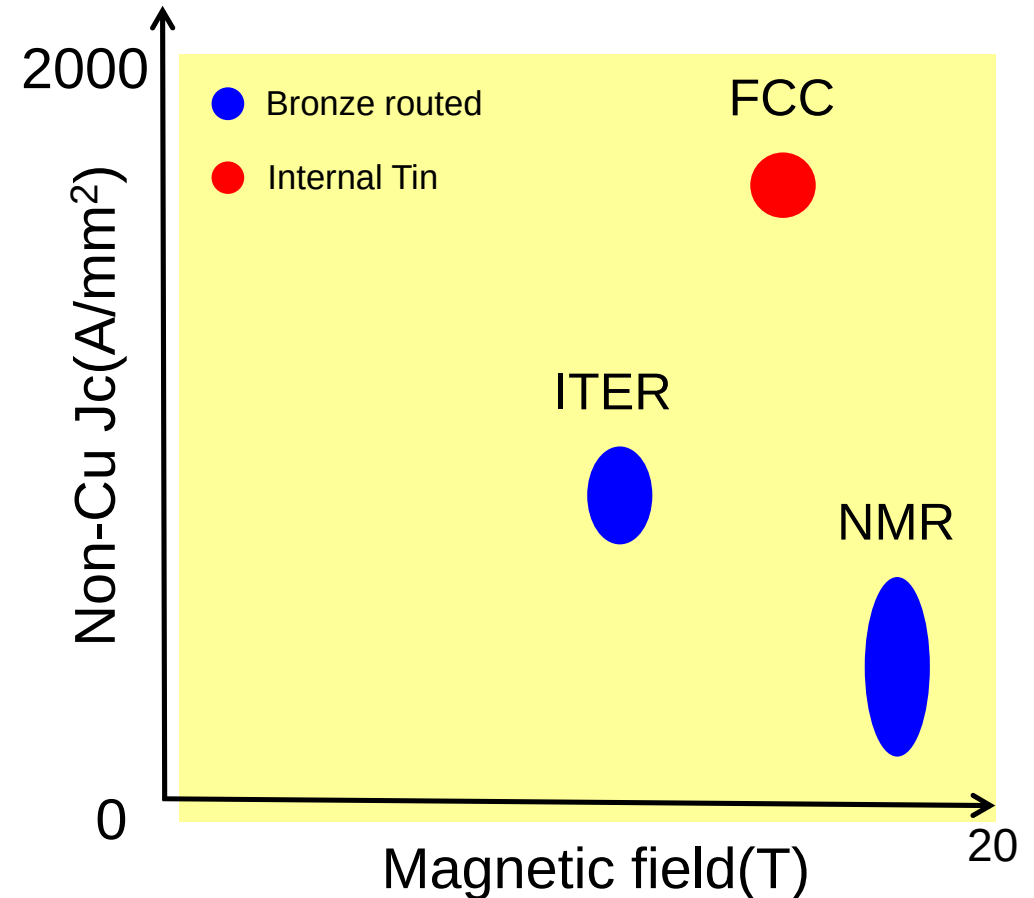
Field :12T-13T

700 (TF) ~ 1,100 (CS) A/mm<sup>2</sup>

## ◆ FCC(Accelerator)

Field: 16T

Non Cu Jc: **Target** 1,500A/mm<sup>2</sup>



“ application driven development”

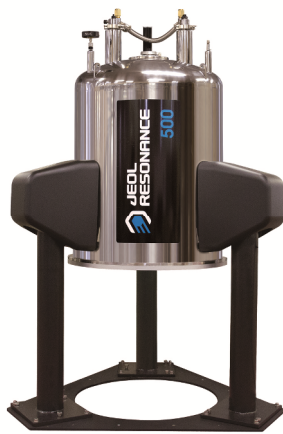
# Nb<sub>3</sub>Sn wire for NMR magnet



# NMR magnet



400MHz(9.4T)



500MHz(11.7T)



600MHz(14.1T)



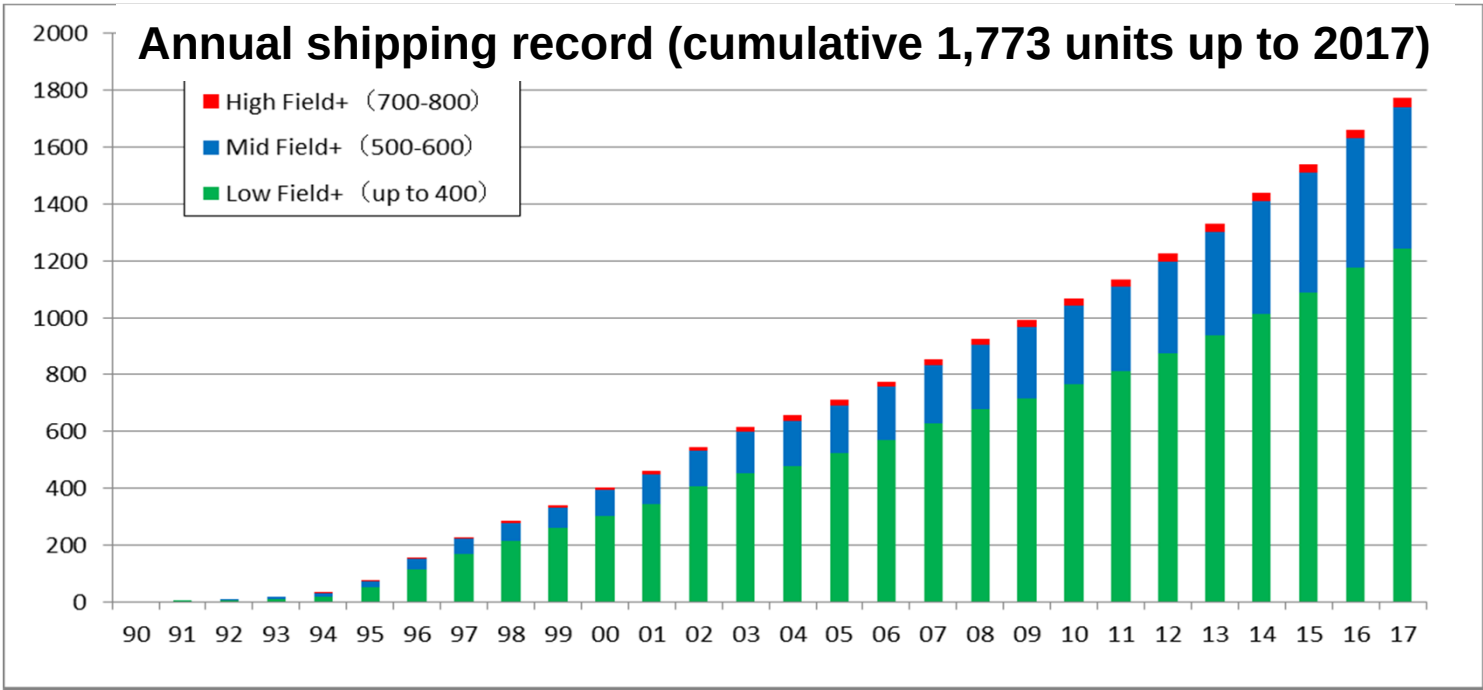
700MHz(16.4T)



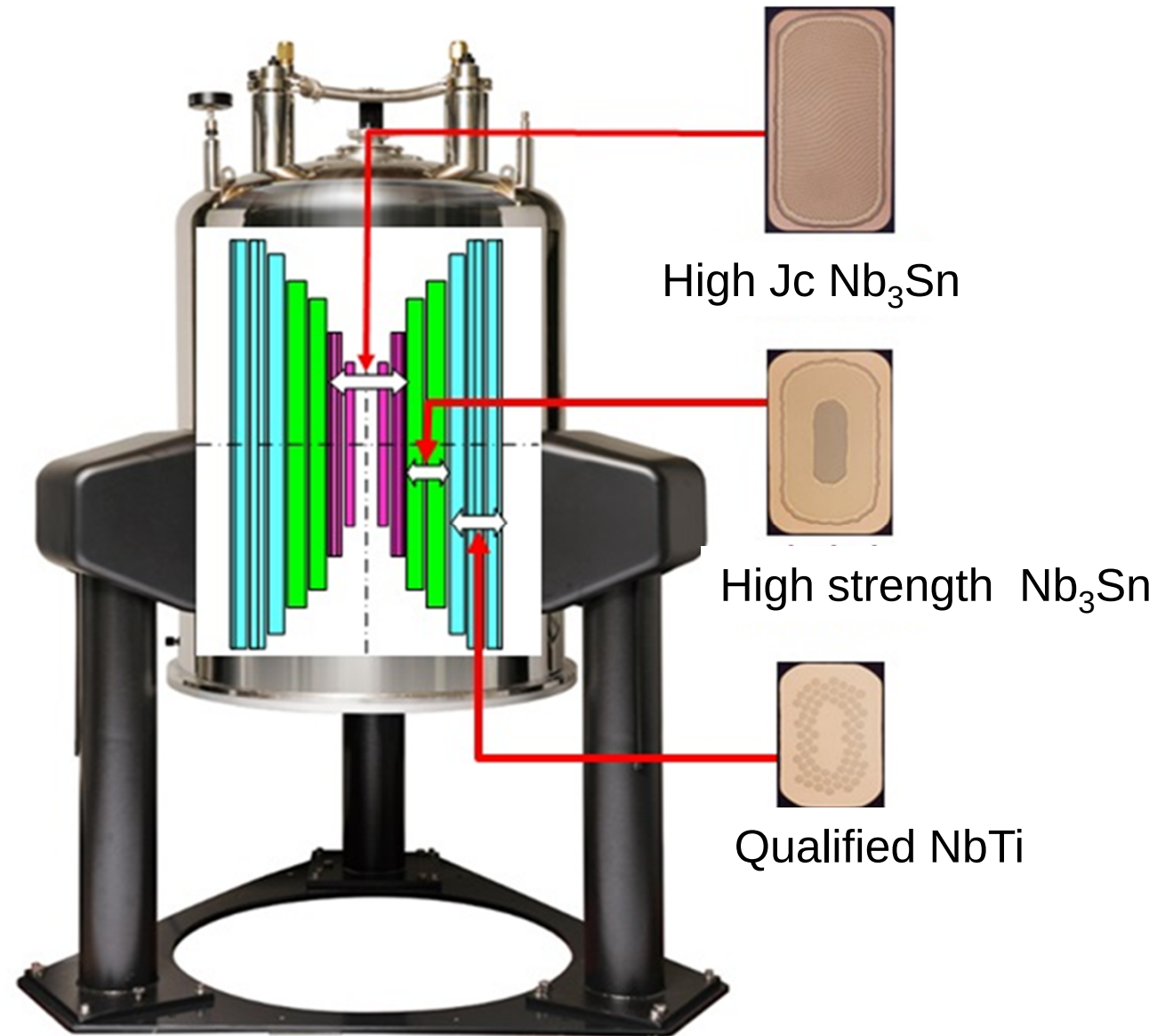
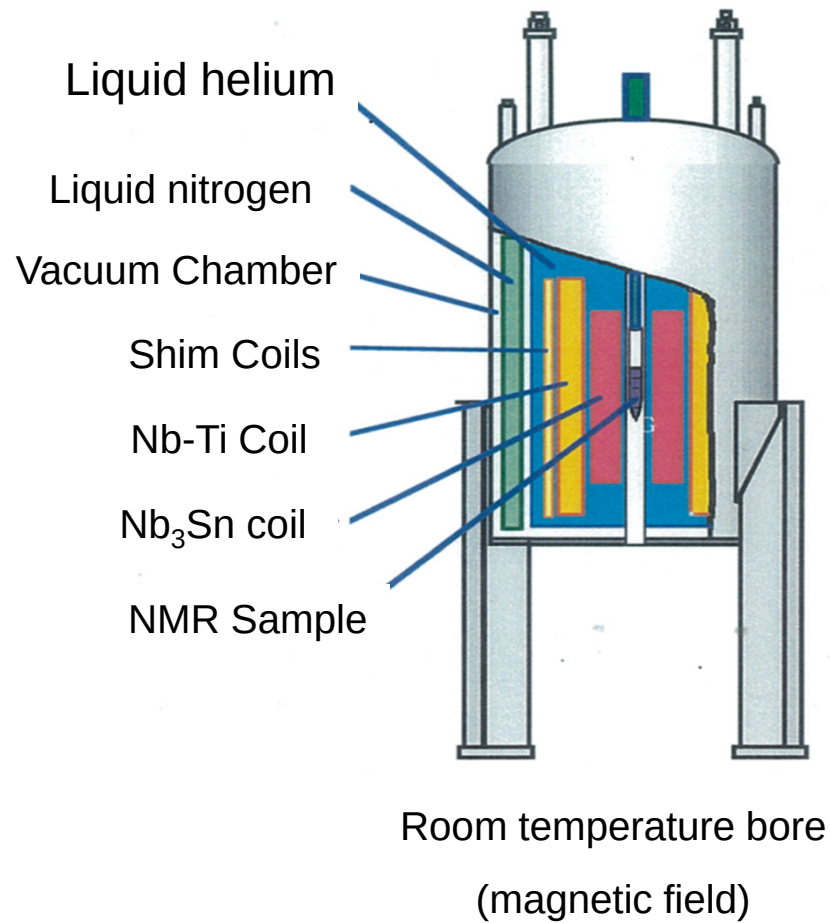
800MHz(18.8T)



1020MHz(24T)

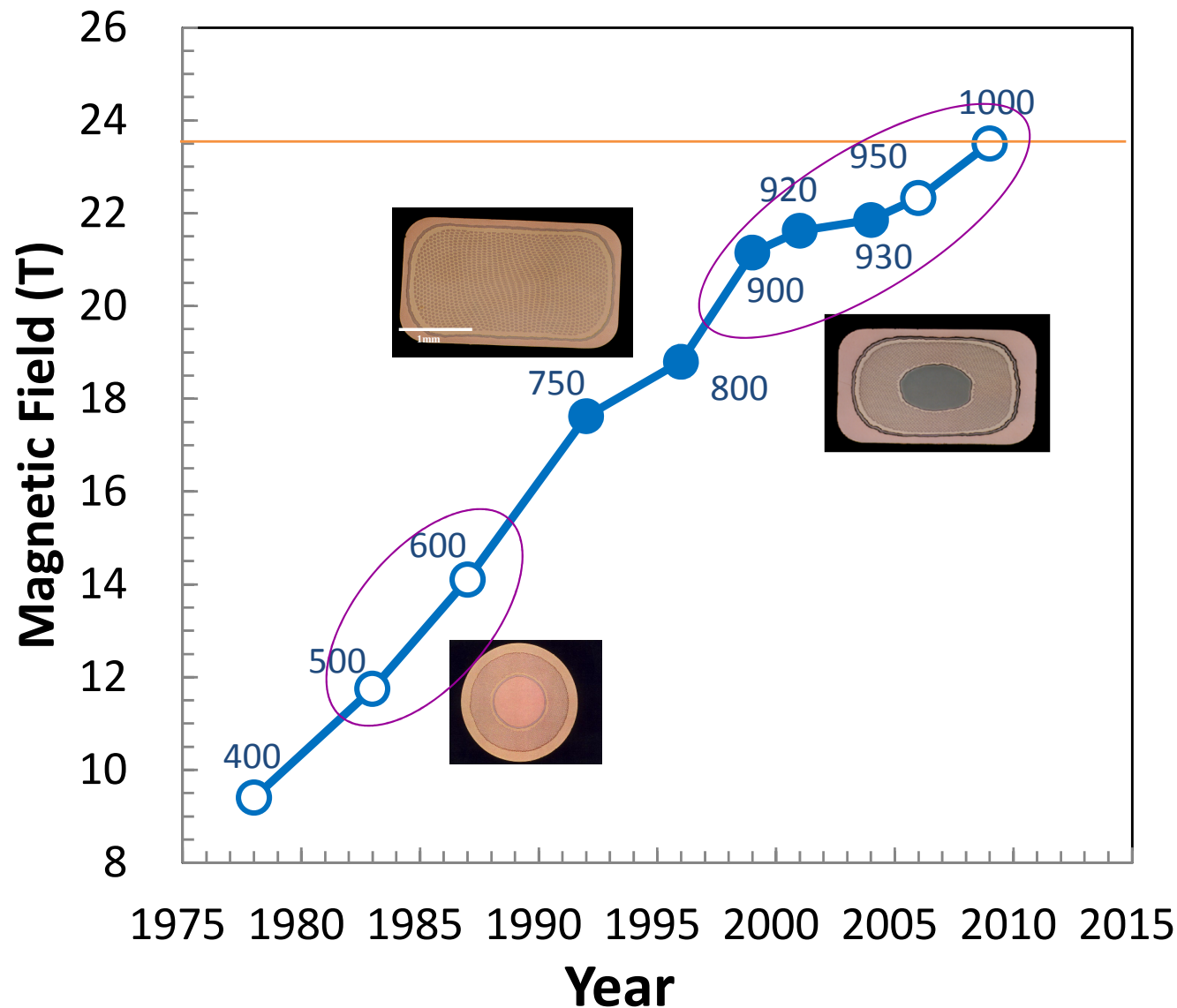


# high field NMR magnet





# Development of Nb<sub>3</sub>Sn wires of Bronze routed type



- ◆ **500/600MHz magnet:**  
**Internal stabilized wire**
- ◆ **750MHz magnet:**  
**Rectangular wire**
- ◆ **900MHz magnet:**  
**High  $J_c$  wire**  
**High strength wire**
- ◆ **950-1,000 MHz magnet:**  
**High Sn wire**
- ◆ **Improvement in  $n$ -value**

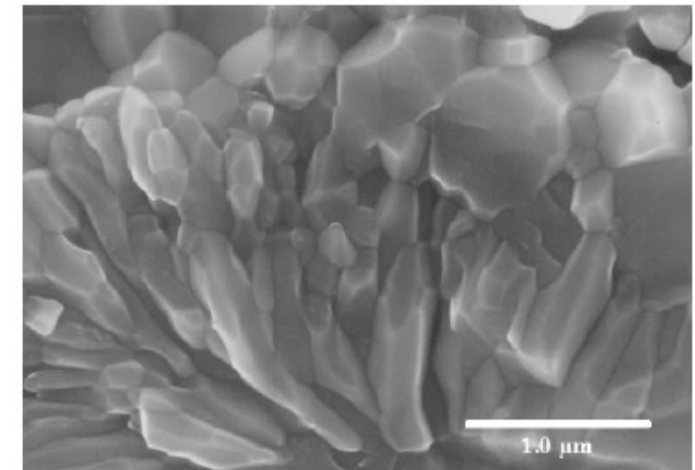
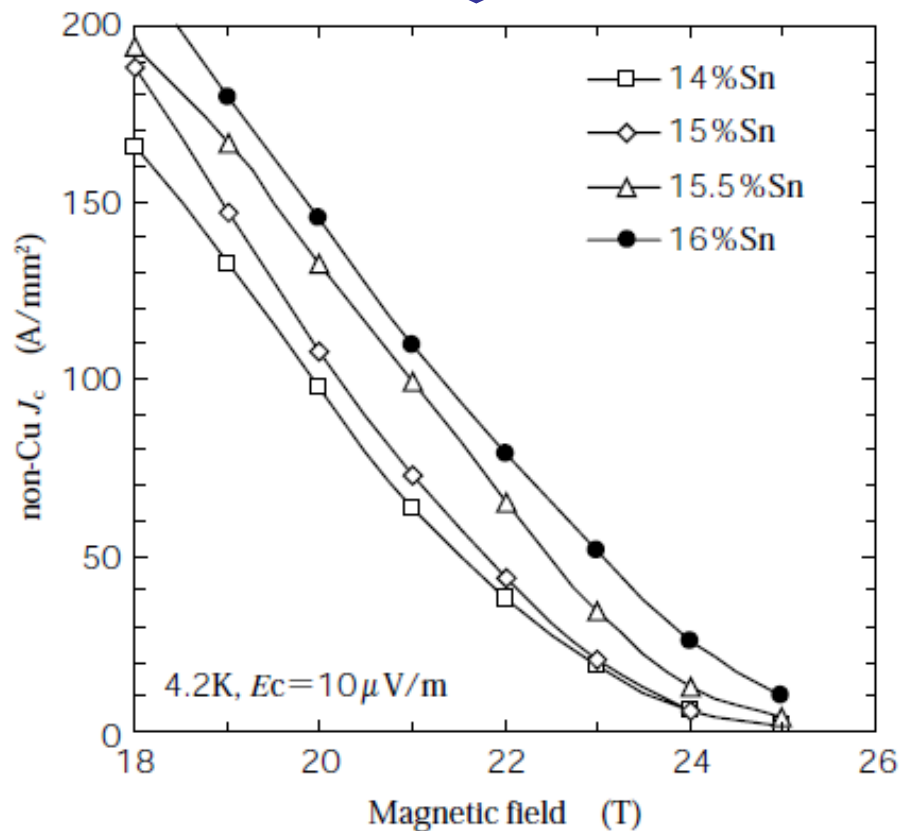
# Jc increase by using high Sn contents Cu-Sn Alloy

Effect of higher Sn content in Cu-Sn alloy

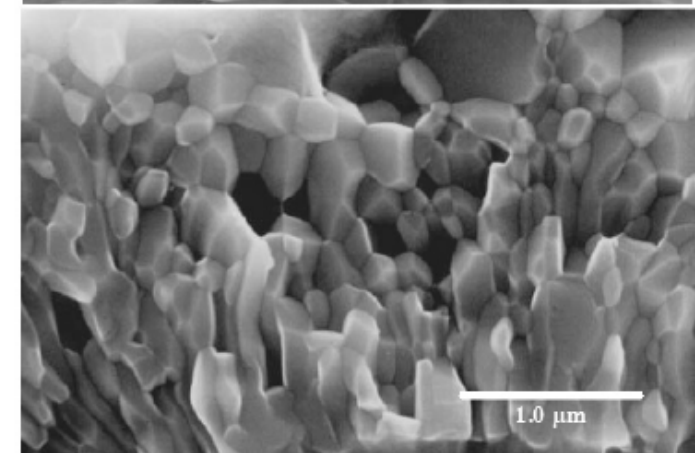
Increasing Nb<sub>3</sub>Sn volume fraction,

better stoichiometry

decrease grain size



14%

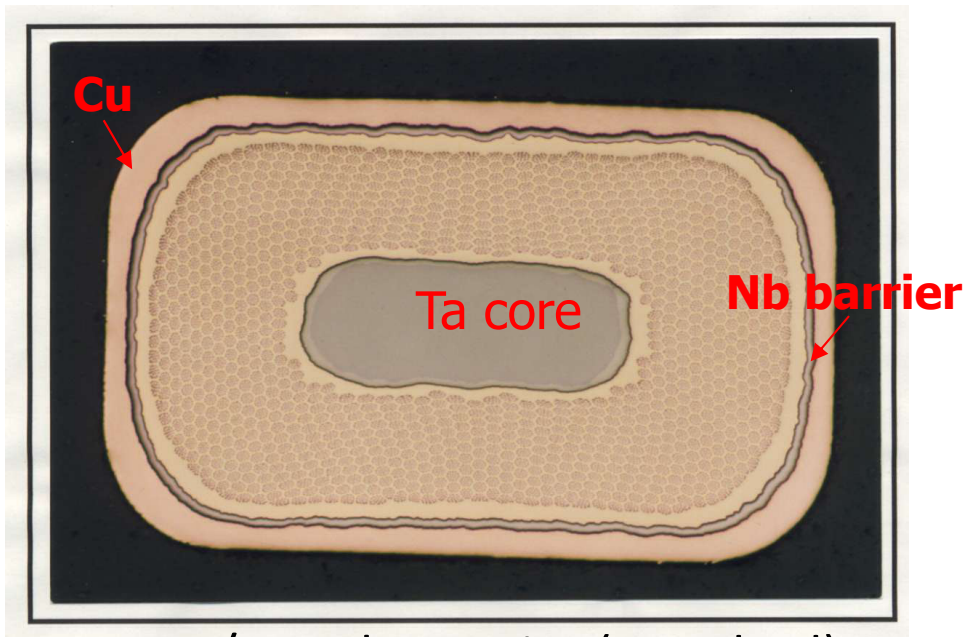


16%

Fracture cross section of  
Nb<sub>3</sub>Sn filament

# Higher strength Nb<sub>3</sub>Sn wire (1)

- ◆ High strength wires with reinforced materials have been developed by several companies/institutes.
- ◆ JASTEC has developed a **Ta reinforced Nb<sub>3</sub>Sn wire** with yield strength (YS) beyond 300MPa at 4.2K. (YS of Ordinary Nb<sub>3</sub>Sn wire: 180MPa at 4K)



T20/0.5 Nb<sub>3</sub>Sn wire (Standard)

- (Cu+Ta)/SC ratio : 0.5
- Number of filament : 20,292
- 0.2% proof strength : >280MPa

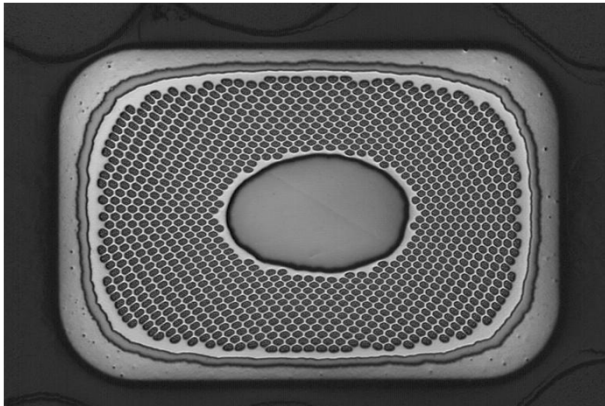
Ta as a reinforcement material has :

- Good workability in cold drawing
- High YS at cryogenic temperatures
- High YS even after Nb<sub>3</sub>Sn

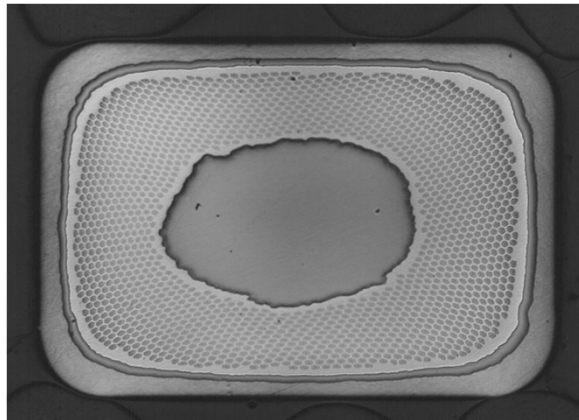
formation heat treatment

# Higher strength Nb<sub>3</sub>Sn wire (2)

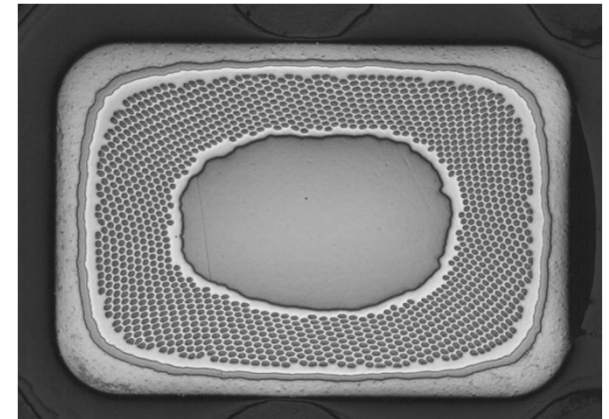
- ◆ The YS of Ta reinforced Nb<sub>3</sub>Sn wire can be controlled by a volume fraction of Ta.



T20/0.5



T30/0.6



T26/0.8

|                            | T20/0.5 | T30/0.6 | T26/0.8 |
|----------------------------|---------|---------|---------|
| Volume fraction of Ta core | ~ 11%   | ~ 17%   | ~ 24%   |
| Yield strength (MPa) @4.2K | ~ 300   | ~ 340   | ~ 400   |

# Nb<sub>3</sub>Sn wire for ITER coils



# ITER (International Thermal nuclear fusion Experimental Reactor)

■ Japan, EU, US, Russia, China, South Korea, India

■ Site : Cadarache, France

■ 2007-2024 Construction

2025 First plasma

2025-2042 Operation

■ TF coil: 420 ton (Japan 105 ton)

(to confine tokamak plasma )

wire procurement: 2009~2012

#2,3 = 40tons: JASTEC #1,4,5:Hitachi

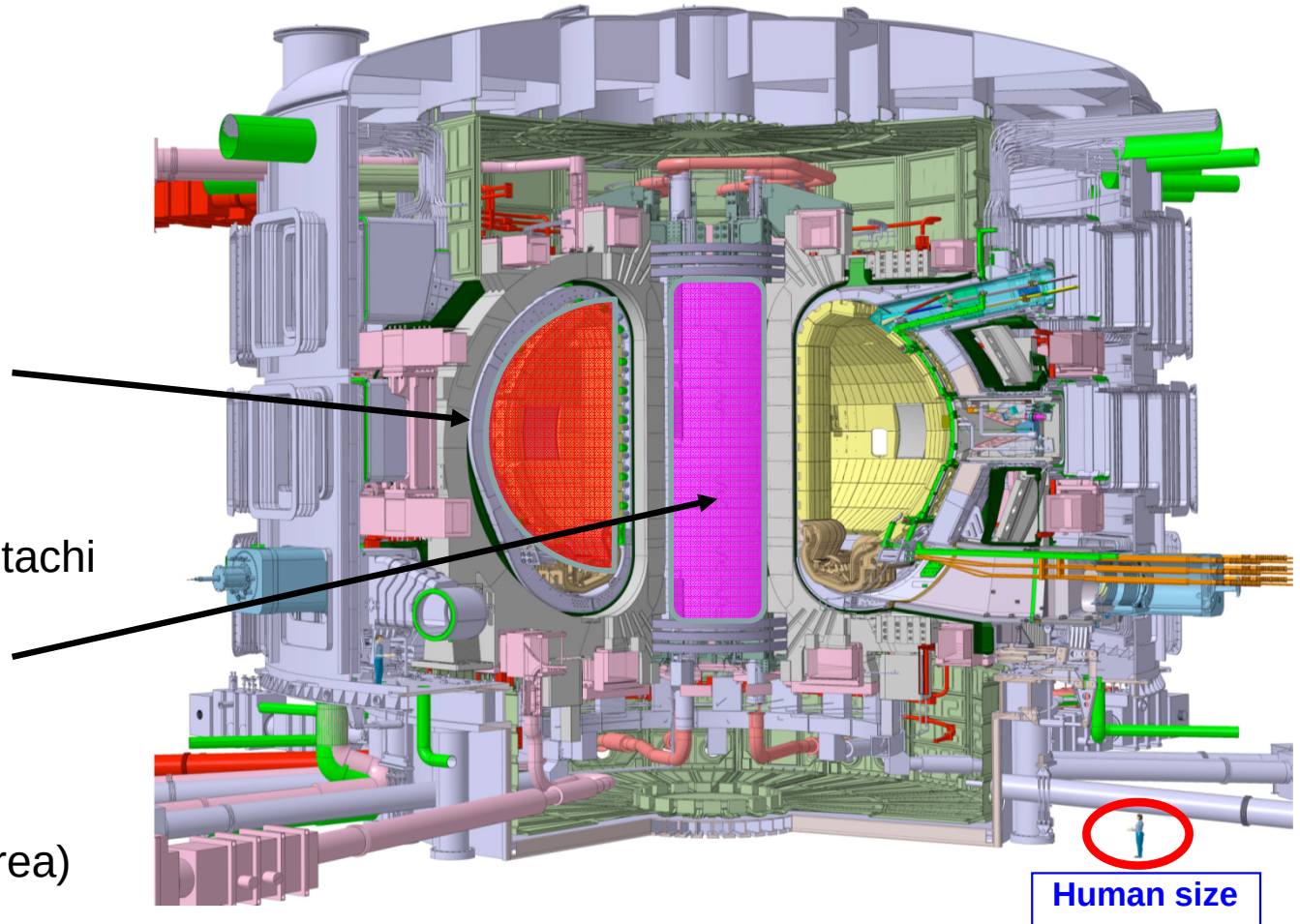
■ CS coil: 120 ton (Japan 120 ton)

(to induce plasma current )

wire procurement: 2012~2016)

#1,2,6 = 60tons : JASTEC

#3,7:Furukawa #4,5:KAT (South Korea)



***JASTEC, having share of 41% in Japan,  
is one of the leading suppliers of Nb<sub>3</sub>Sn conductor to ITER.***

# Nb<sub>3</sub>Sn wire development for CS coil

Parameters for TF coil and CS coil

| Parameters                    | TF   | CS |
|-------------------------------|------|----|
| Nominal Peak field (kA)       | 68   | 45 |
| Maximum Operating Current (T) | 11.8 | 13 |

N. Mitchell *et al*; *IEEE Trans. Appl. Supercond.* 22(2012), 4200809

**Table 1** Required specifications of Nb<sub>3</sub>Sn strand for ITER

| Item                  | Strand for TF coils          | Strand for CS coils          | Remarks                        |
|-----------------------|------------------------------|------------------------------|--------------------------------|
| Strand diameter       | $0.820 \pm 0.006 \text{ mm}$ | $0.830 \pm 0.005 \text{ mm}$ | After Cr plating               |
| Cu to nonCu ratio     | $1.0 \pm 0.1$                |                              |                                |
| RRR                   | $> 100$                      |                              |                                |
| nonCu $J_c$           | $> 700 \text{ A/mm}^2$       | $> 750 \text{ A/mm}^2$       | at 4.2K, 12T                   |
| n-value               | $> 20$                       |                              | at 4.2K, 12T                   |
| nonCu hysteresis loss | $< 1,000 \text{ mJ/cm}^3$    |                              | at 4.2K, $\pm 3\text{T}$ cycle |

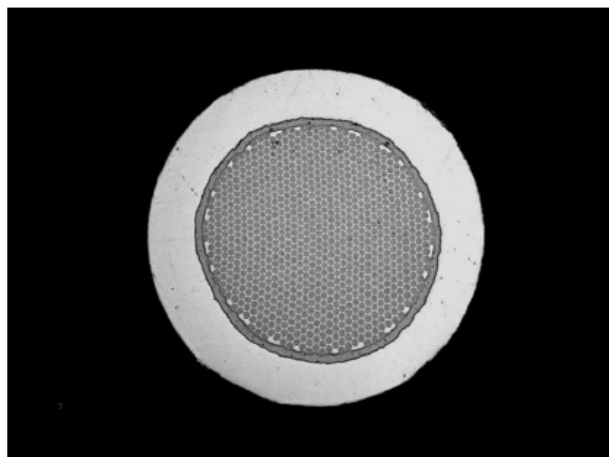
N. Murakami *et al*; *Kobe Steel Engineering Reports*, 59(1),36(2009)

*Comparing with TF coil, CS coil required higher  $J_c$  to Nb<sub>3</sub>Sn wire (strand)*

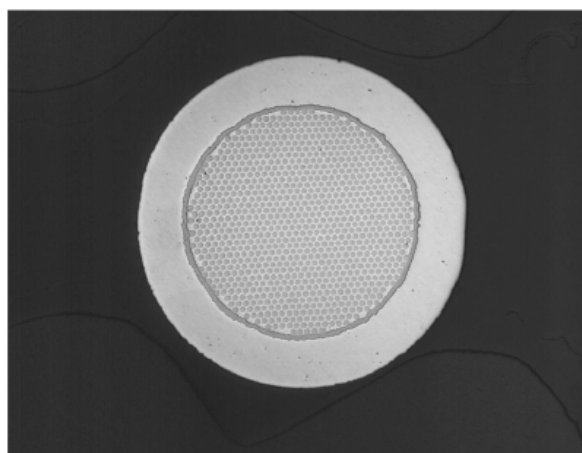
# Nb<sub>3</sub>Sn wire development for CS coil

WIRE PARAMETERS OF SAMPLES

| Sample                 | GTS-I  | GTS-J  | GNS-J  | GNB-J  | G-TF-I | GTSM-I | GNSM-J |
|------------------------|--------|--------|--------|--------|--------|--------|--------|
| Wire diameter (mm)     | 0.818  | 0.818  | 0.818  | 0.818  | 0.826  | 0.826  | 0.815  |
| Cu ratio               | 0.96   | 0.96   | 0.94   | 0.91   | 0.91   | 0.93   | 0.93   |
| Filament number        | 16,891 | 16,891 | 16,891 | 7,999  | 12,787 | 17,347 | 16,891 |
| Filament diameter (μm) | 2.3    | 2.3    | 2.3    | 3.4    | 2.7    | 2.3    | 2.3    |
| Barrier material       | Ta/Nb  | Ta/Nb  | Nb     | Nb     | Nb     | Ta/Nb  | Nb     |
| Barrier thickness (μm) | 15     | 15     | 15     | 15     | 7      | 9      | 7      |
| Heat-treatment pattern | Type-I | Type-J | Type-J | Type-J | Type-I | Type-I | Type-J |



(a) GNS-J with barrier thickness of 15μm



(b) GTSM-I with barrier thickness of 9μm

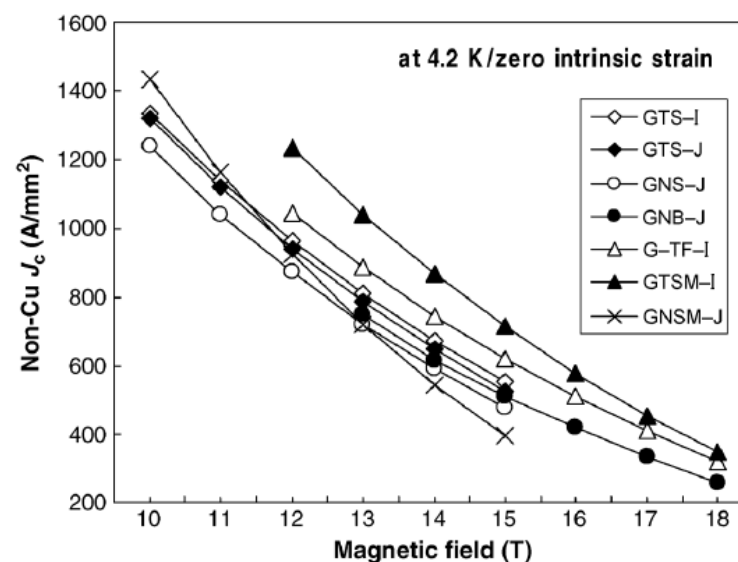


Fig. 3. Magnetic field dependence on non-Cu critical current density at 4.2 K and zero intrinsic strain for all samples.

## Key Factors

- ✓ Filament diameter
- ✓ Heat treatment
- ✓ Barrier thickness
- ✓ Barrier material



Non-Copper Jc > 1100 A/mm² @ 12T

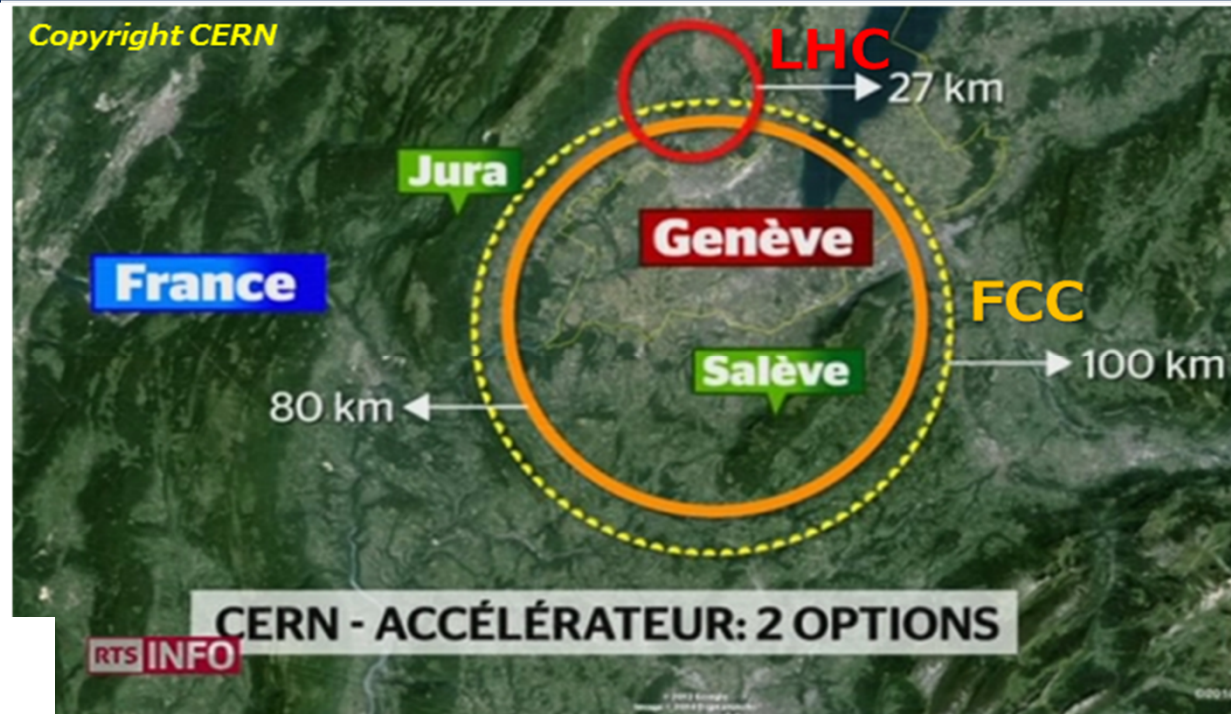
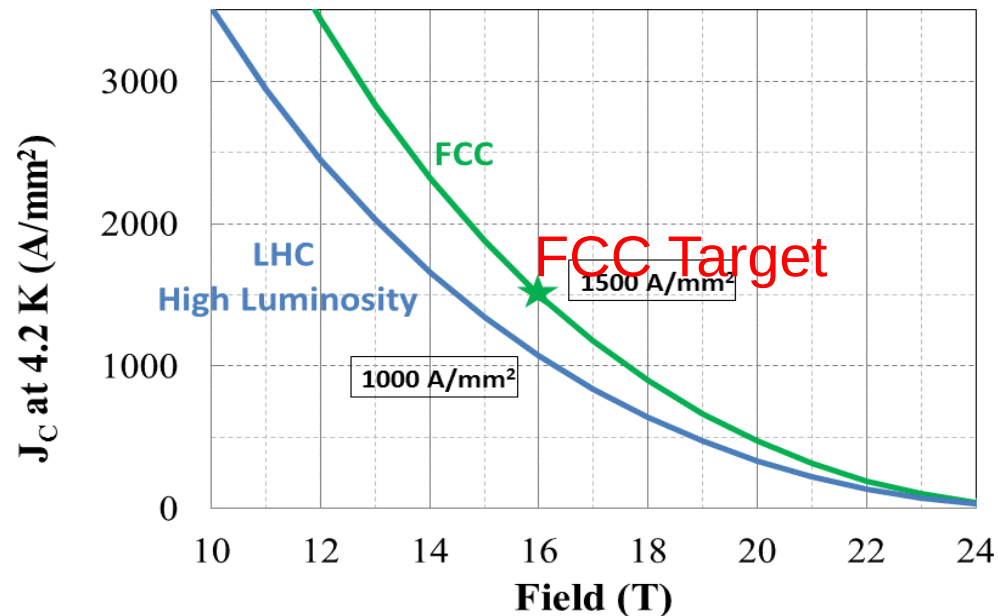
T. Miyatake et al; IEEE Trans. Appl. Supercond. 22(2012), 4805005

# Nb<sub>3</sub>Sn wire for FCC



# FCC (Future Circular Collider)

High  $J_c$  Nb3Sn for FCC



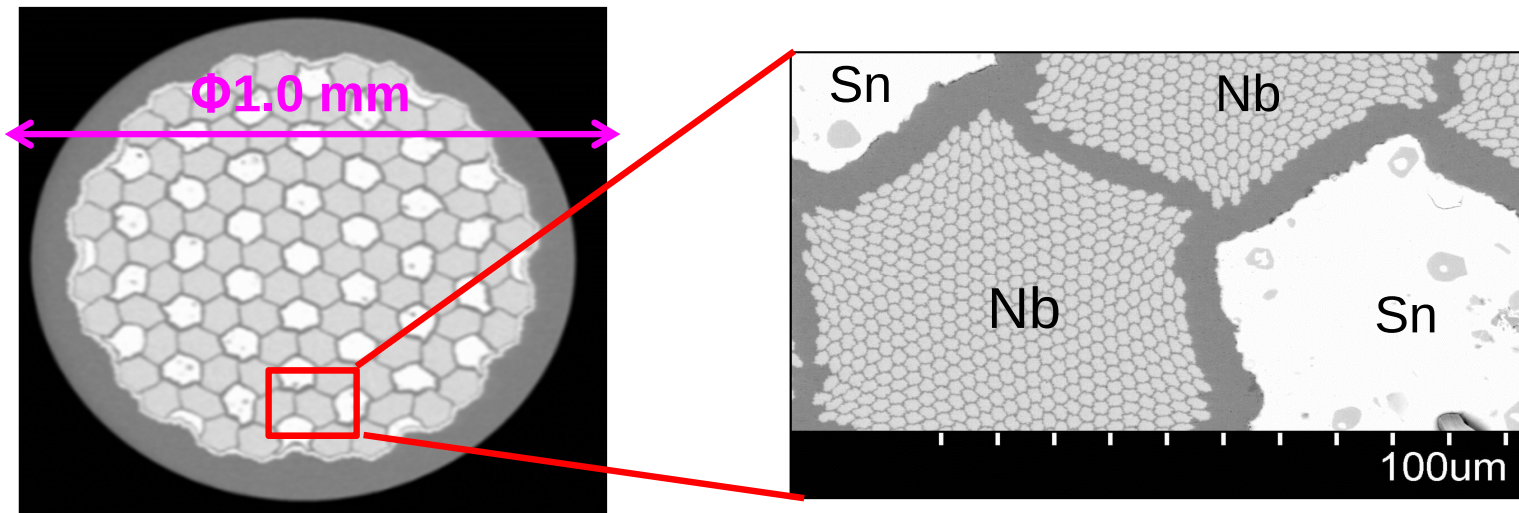
The target value: non Cu  $J_c$  : **1500 A/mm² at 4.2 K, 16 T**. It needs 50 % increase than that for HL-LHC.



# Key factors for higher $J_c$ Nb<sub>3</sub>Sn

For FCC, Distributed Tin (DT) method with higher Sn concentration is under development.

Cross-section of DT wire (before Heat treatment)



- Nb sub-element
- Monocore Sn
- Nb common barrier
- Stabilized Cu outside barrier

**For higher  $J_c$ ...**

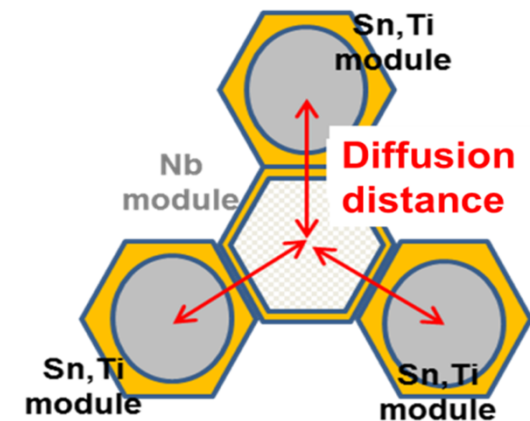
- (1) Improvement in Sn diffusion : Reduction of Sn diffusion distance
- (2) Increase in Nb volume fraction: Reduction of useless volume
- (3) Ternary additive elements : Control of  $B_{c2}$
- (4) Optimization of heat treatment : Stoichiometry, Refinement

# Experiment

## @Sample parameters

|                                         | 1A   | 1B   | 1C   | 2A   | 2B   |
|-----------------------------------------|------|------|------|------|------|
| Wire Dia. (mm)                          | 0.80 | 0.75 | 0.64 | 0.80 | 0.80 |
| Nb ratio (%)                            | 47.1 | 47.1 | 47.1 | 48.0 | 48.0 |
| Dia. Nb Fila. ( $\mu\text{m}$ )         | 2.0  | 1.8  | 1.6  | 1.2  | 1.2  |
| Dia. Nb module ( $\mu\text{m}$ )        | 60   | 56   | 48   | 32   | 32   |
| Sn diffusion distance ( $\mu\text{m}$ ) | 60   | 56   | 48   | 32   | 32   |
| Ti ratio (%)                            | 0.55 | 0.55 | 0.55 | 0.48 | 0.35 |
| Cu/non-Cu ratio                         | 0.34 | 0.34 | 0.34 | 1.0  | 1.0  |

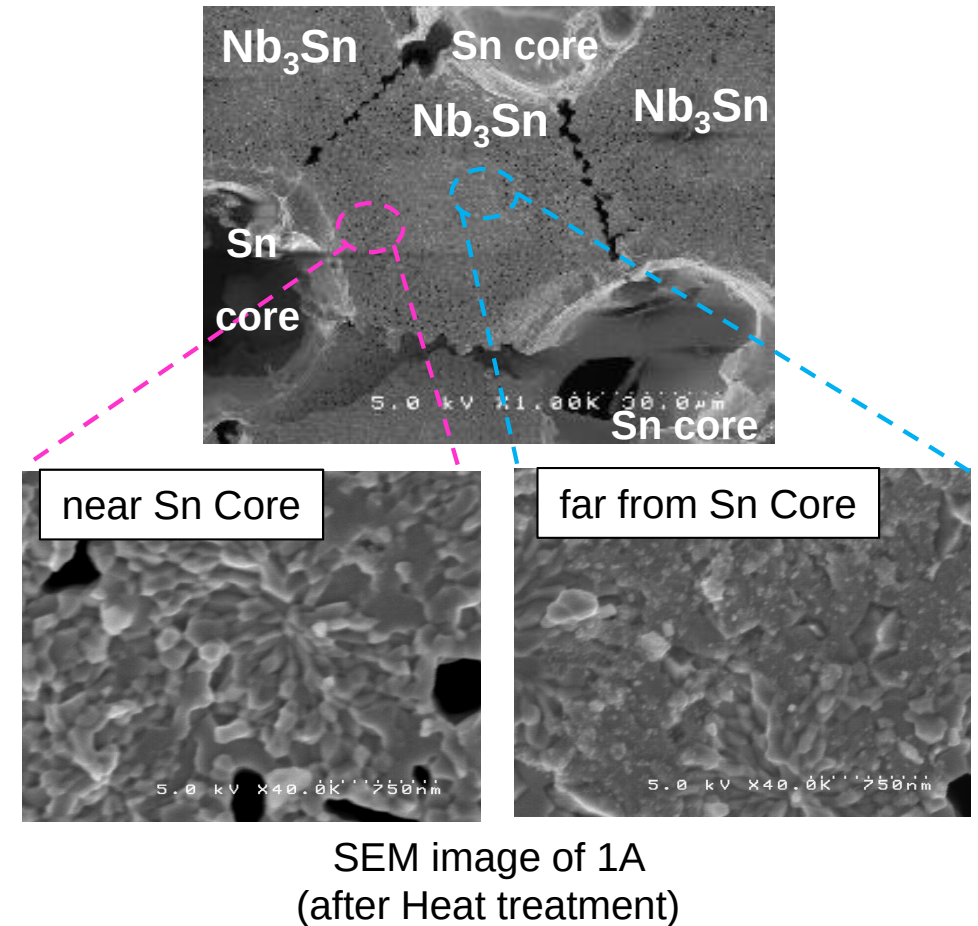
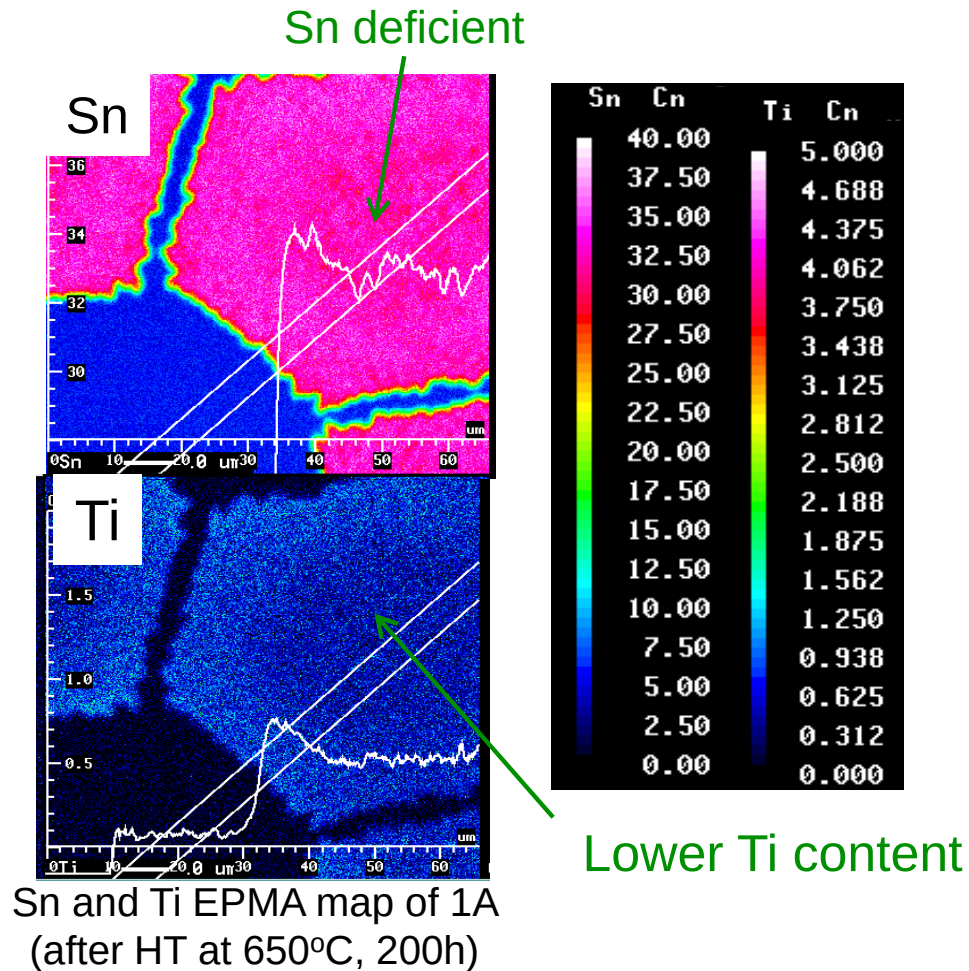
- We prepared 5 samples focusing on Sn diffusion distance and Ti contents.
- 1A, 1B and 1C have the same design excepting Sn diffusion distance.
- 2A and 2B were reduced the Ti content compared to 1C.



【Definition of Sn diffusion distance】

# Improvement in Sn diffusion

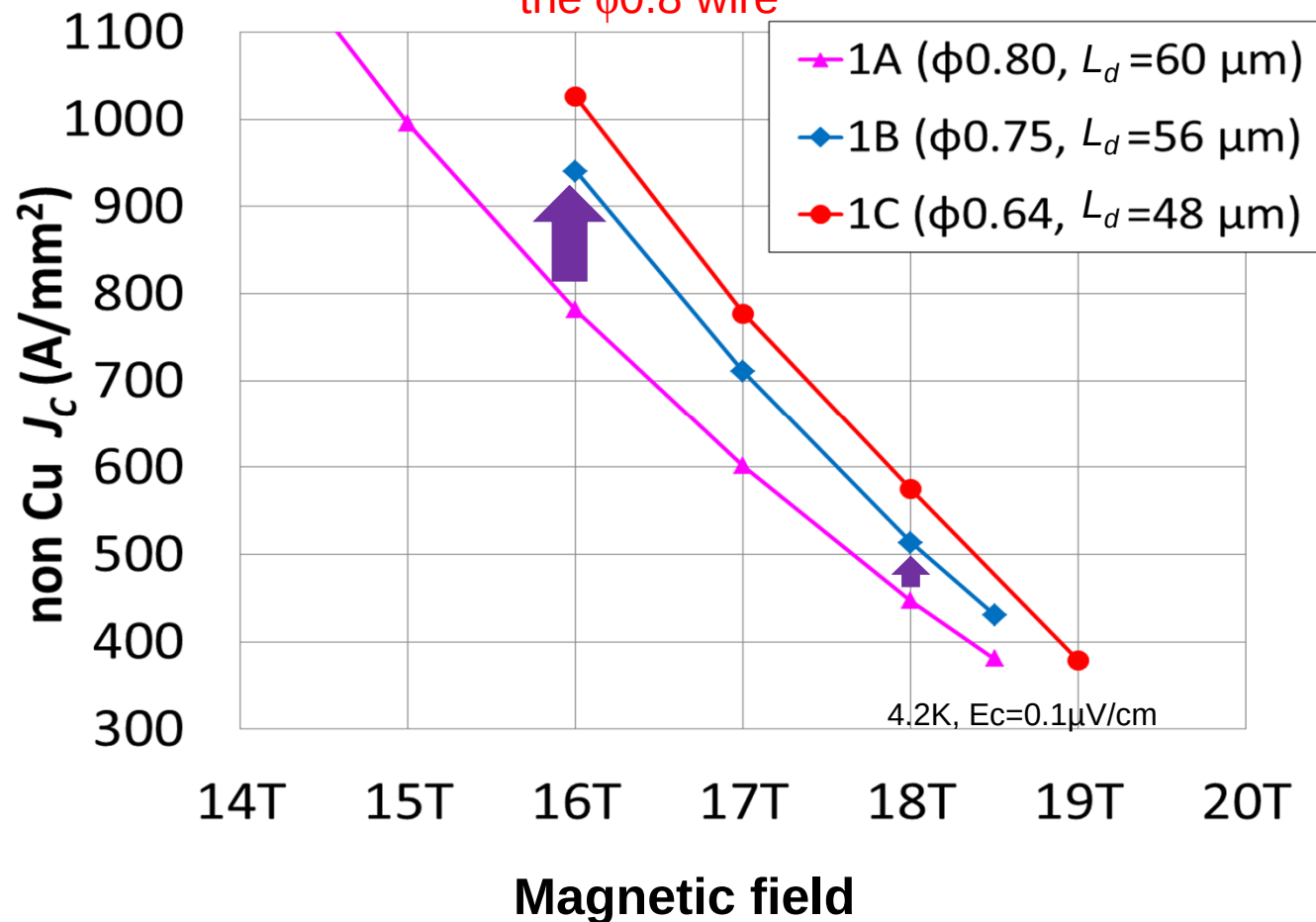
Sn diffusion is one of key factors to achieve higher  $J_c$



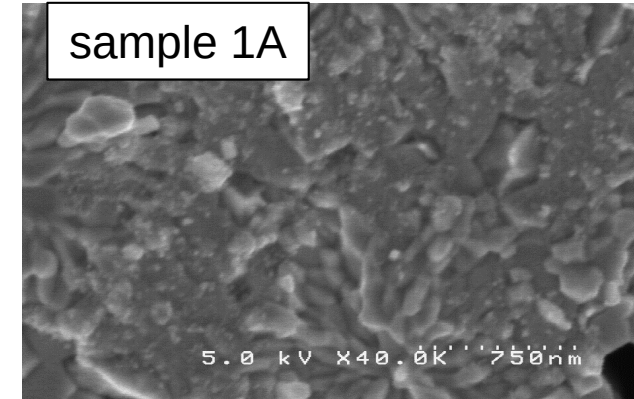
Long diffusion distance of Sn  $\Rightarrow$  lack of Sn and Ti in Nb module  
 $\Rightarrow$  larger grain size at the center.

# Improvement in Sn diffusion

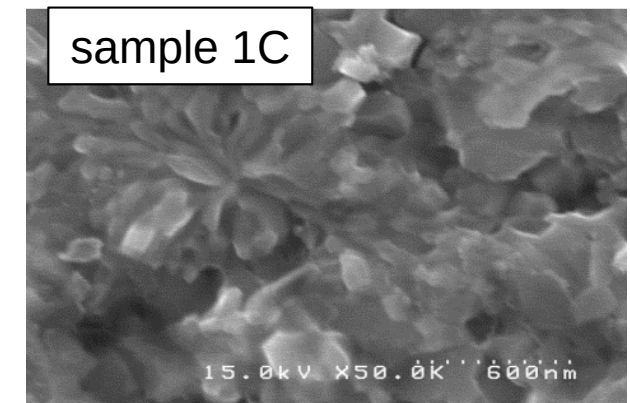
Sn diffusion distance ( $L_d$ ) was reduced by drawing down the  $\phi 0.8$  wire



Before Sn diffusion improvement



After Sn diffusion improvement



SEM image of A15 area far from Sn core before/after Sn diffusion improvement

Reduction in Sn diffusion distance can improve  $J_c$  by 28%.

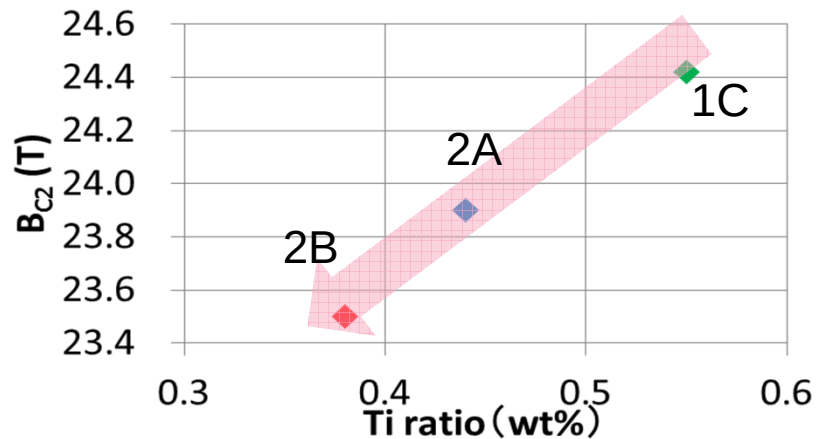
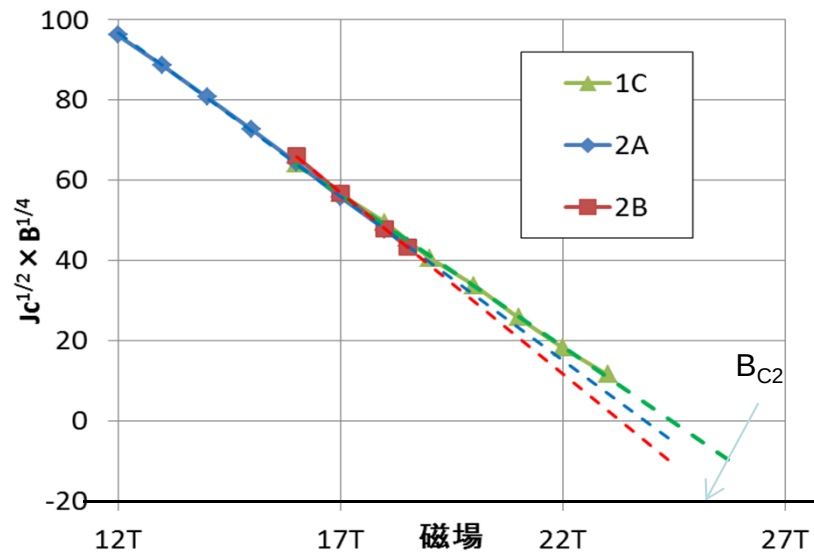
non Cu  $J_c = 1025 \text{ A/mm}^2$  @ 16 T.



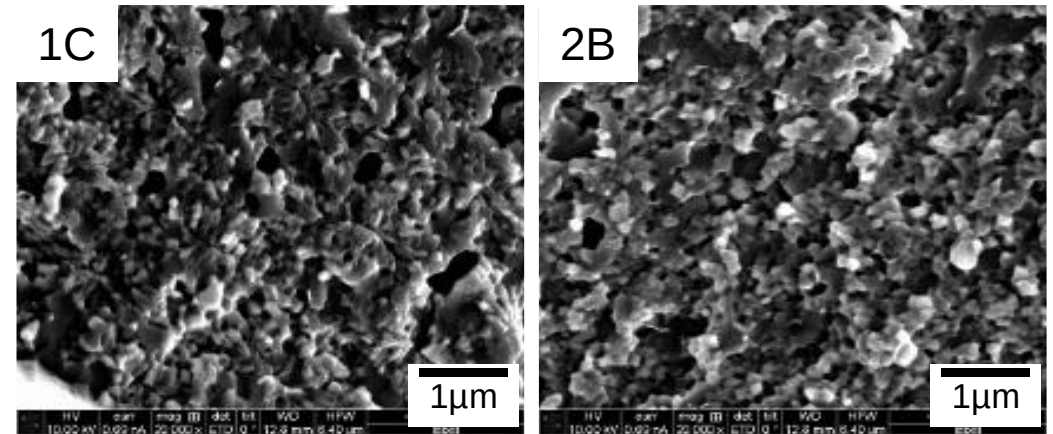
# Ternary additive elements

## ① Control of $B_{C2}$

Kramer Plot



## ② $Nb_3Sn$ grains



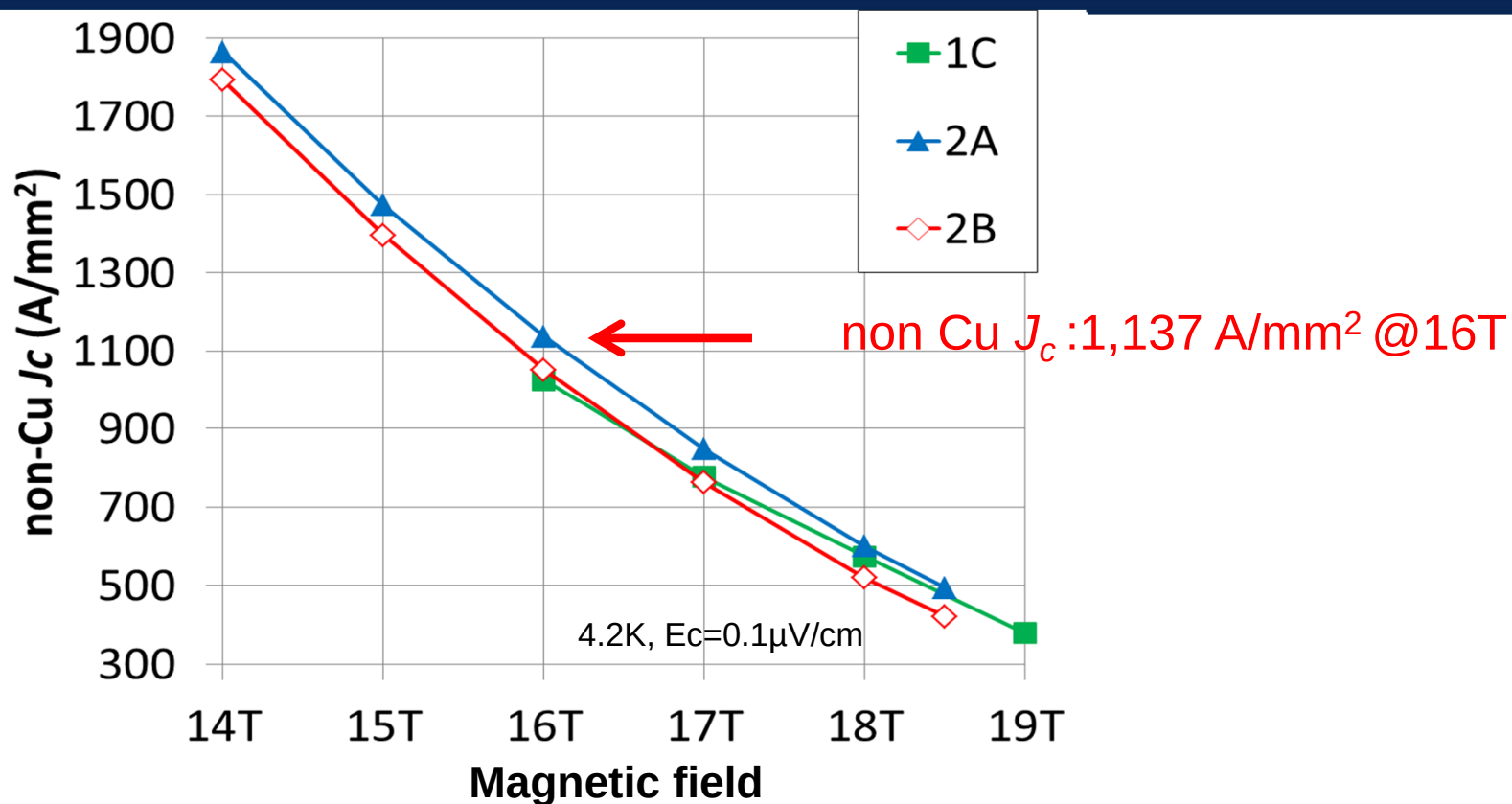
|    | Aspect ratio * of $Nb_3Sn$ | Average grain size of $Nb_3Sn$ |
|----|----------------------------|--------------------------------|
| 1C | 2.1                        | 181nm                          |
| 2A | 1.7                        | 188nm                          |
| 2B | 1.7                        | 200nm                          |

\* Aspect ratio  $\div 1 \rightarrow$  Equiaxed grains  $\rightarrow$  High  $J_c$

- There is no negative influence such as coarsening of  $Nb_3Sn$  grains due to Ti reduction
- By decreasing Ti contents, we **suppress  $B_{C2}$** . (In descending order of Ti amount: 1C > 2A > 2B).



# Ternary additive elements



|                                       | 1C   | 2A   | 2B   |
|---------------------------------------|------|------|------|
| Wire Dia. (mm)                        | 0.64 | 0.80 | 0.80 |
| Sn diffusion distance (μm)            | 48   | 32   | 32   |
| Ti ratio (%)                          | 0.55 | 0.48 | 0.35 |
| non Cu $J_c$ (A/mm <sup>2</sup> )@16T | 1025 | 1137 | 1032 |

Lower Ti content is not necessarily harmful when Sn diffusion distance is short enough.

# Short summary

- We have achieved non Cu  $J_c$  @16T up to 1,137A/mm<sup>2</sup>,  
by improving Sn diffusion and controlling Ti content.  
 $J_c$  value is approaching to the target for 16T magnets for FCC.
- The following items will be addressed to attain the provisional  $J_c$  target of 1,200A/mm<sup>2</sup>:
  - (1) Control ternary additive element (further reduction of Ti, Ti doping method)
  - (2) Increase in Nb area ratio (by decreasing Cu inside barrier)
  - (3) Further refinement of Nb<sub>3</sub>Sn grains by controlling heat-treatment condition



Thank you for your attention !